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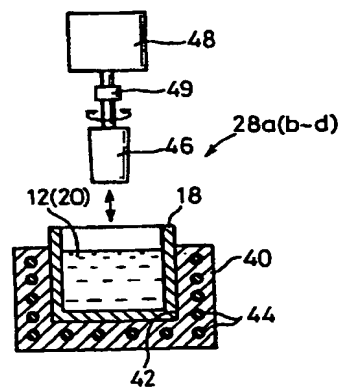
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**(54) METHOD AND APPARATUS FOR MANUFACTURING SEMI-SOLIDIFIED METAL**

(57) A predetermined amount of molten metal 12 is supplied to a heat-insulating crucible 18. After that, a chill block 46, which is cooled to a predetermined temperature of not more than a temperature of the molten metal 12, is immersed and rotated in the molten metal 12. Accordingly, the molten metal 12 is agitated while being cooled to give no directivity of cooling. It is possible to obtain semisolidified metal 20 which is formed into slurry uniformly and effectively as a whole. The semisolidified metal 20 is discharged from the heat-insulating crucible 18, and it is supplied to a forming machine 22 to apply a forming treatment thereto. Accordingly, it is possible to produce the desired slurry efficiently and economically.

**FIG. 4**



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## Description

### TECHNICAL FIELD

[0001] The present invention relates to a method and an apparatus for producing semisolidified metal to obtain predetermined slurry from molten metal.

### BACKGROUND ART

[0002] An operation is generally performed to produce semisolidified metal, i.e., slurry in an amount of one shot for the forming process, by using molten metal of, for example, aluminum, magnesium, or alloy thereof. It is known that a forming operation based on the use of slurry especially has such an advantage that the surface accuracy of a formed product is excellent. In order to produce such slurry, for example, the thixocasting process and the rheocasting process are widely adopted.

[0003] However, in the case of the thixocasting process described above, it is necessary to use an exclusive billet and a reheating apparatus. For this reason, the following problems are pointed out. That is, the material cost and the equipment cost are considerably expensive, and the entire production operation is complicated.

[0004] On the other hand, in the rheocasting process, the mass production is performed based on the continuous batch system. In this process, the cooling is performed by discharging the molten metal while allowing the molten metal to make contact with a cooling section cooled with water. Therefore, the temperature of slurry differs between the start and the end of the cooling. A problem arises in that the temperature of the slurry is not managed accurately.

[0005] A method is also known, in which slurry is produced in accordance with cooling, heating, and agitation in a forming machine. However, the following inconveniences arise. That is, the cycle time is prolonged, and especially the shot weight is increased.

[0006] When the produced slurry is supplied into the forming machine, a container for accommodating the slurry is usually inverted in the vertical direction. However, it is difficult to discharge the entire amount of slurry in the container, for example, due to the temperature of the slurry in the container, the shape of the container, and the weight of the slurry. As a result, the following problems are pointed out. That is, remaining matters of the slurry appear in the container, and the supply weight of the slurry is dispersed. Further, the slurry, which is newly produced in the container, is badly affected thereby.

[0007] When different parts are formed, the shot weight differs depending thereon. Therefore, the following problems are pointed out. That is, it is impossible to correctly manage the temperature of the slurry. When the shot weight is increased, it takes a long time to per-

form the operation for producing the slurry. It is difficult to efficiently perform the forming operation for a variety of different parts to give high qualities.

[0008] An object of the present invention is to provide a method and an apparatus for producing semisolidified metal, which make it possible to produce desired slurry efficiently and economically.

[0009] Another object of the present invention is to provide an apparatus for producing semisolidified metal, which makes it possible to economically produce desired slurry and easily discharge the slurry in a reliable manner.

[0010] Still another object of the present invention is to provide an apparatus for producing semisolidified metal, which makes it possible to economically produce various slurries having different weight so that they have high qualities, wherein the system is simplified.

### DISCLOSURE OF THE INVENTION

[0011] According to the present invention, a predetermined amount of molten metal is supplied to a heat-insulating crucible. After that, the molten metal in the crucible is cooled by the aid of a cooling member which is cooled to be at a predetermined temperature of not more than a temperature of the molten metal. Simultaneously, the molten metal is agitated. Accordingly, in the heat-insulating crucible, the molten metal is reliably formed into slurry generally uniformly as a whole without involving any directivity of cooling. Thus, the reheating is unnecessary, and it is possible to efficiently obtain desired semisolidified metal.

[0012] According to the present invention, a predetermined amount of molten metal is supplied to a heat-insulating crucible, and then the molten metal in the crucible is cooled by the aid of a cooling member which is cooled to be at a predetermined temperature of not more than a temperature of the molten metal. Further, the cooling member is moved in the horizontal direction and/or in the vertical direction while rotating the cooling member. Thus, the molten metal is agitated. For example, the cooling member is moved in a reciprocating manner in the horizontal direction and/or in the vertical direction. Alternatively, the cooling member is moved spirally in the horizontal direction.

[0013] Accordingly, especially when heat-insulating crucibles having various shapes are used, the cooling member is moved along with the shape of the heat-insulating crucible. Thus, the directivity of cooling is excluded to be as less as possible, and the molten metal can be effectively agitated. Accordingly, the molten metal is formed into slurry uniformly and reliably as a whole. It is possible to obtain desired semisolidified metal efficiently with a high quality.

[0014] In the present invention, the semisolidified metal is produced after a predetermined amount of molten metal is supplied to a heat-insulating crucible, by cooling and agitating the molten metal in the heat-insu-

lating crucible by the aid of a plurality of cooling members. Accordingly, even when the shot weight is increased, then the directivity of cooling is avoided to be as less as possible, and it is possible to quickly and smoothly obtain the desired semisolidified metal formed into slurry uniformly and reliably as a whole.

[0015] Further, the cooling members are integrally held by a driving mechanism by the aid of a fixing means in a state in which an arbitrary number of the cooling members are stacked with each other. Therefore, it is enough to change the number of stacked cooling members depending on the change of the shot weight. Thus, it is possible to produce the desired semisolidified metal efficiently to have a high quality. The fixing means includes a shaft member for being integrally inserted into the plurality of stacked cooling members, and a fixture for being screwed on an end of the shaft member. Thus, it is possible to effectively simplify the structure.

[0016] In the present invention, the molten metal is supplied into a heat-insulating crucible, and then a cooling member is immersed in the molten metal. The molten metal is agitated in a state in which a cooling medium having a predetermined temperature is supplied to the inside of the cooling member. Accordingly, the directivity of cooling is avoided to be as less as possible, and it is possible to convert the molten metal into slurry quickly and reliably. Further, when the temperature of the cooling medium is managed, it is unnecessary to reheat the semisolidified metal. Thus, it is possible to efficiently obtain the desired semisolidified metal.

[0017] In the present invention, a predetermined amount of molten metal is supplied to divided type heat-insulating crucibles. After that, the molten metal in the heat-insulating crucibles is cooled and agitated by the aid of a cooling member to produce semisolidified metal. Subsequently, the heat-insulating crucibles are subjected to opening/closing operation by the aid of an opening/closing mechanism. Accordingly, the semisolidified metal in the heat-insulating crucibles falls in accordance with its self-weight, and it is discharged from the heat-insulating crucibles.

[0018] Accordingly, the directivity of cooling is avoided to be as less as possible, and it is possible to obtain the desired semisolidified metal formed into slurry uniformly and reliably as a whole. Further, it is possible to discharge the semisolidified metal from the heat-insulating crucibles smoothly and reliably.

#### BRIEF DESCRIPTION OF THE DRAWINGS

##### [0019]

FIG. 1 shows an illustrative schematic perspective view depicting a production apparatus for carrying out a method for producing semisolidified metal according to a first embodiment of the present

invention.

FIG. 2 shows an illustrative plan view depicting the production apparatus.

FIG. 3 illustrates the operation of a molten metal-ladling robot which constructs the production apparatus.

FIG. 4 illustrates an agitator which constructs the production apparatus.

FIGS. 5A to 5E illustrate a chill block-treating unit for treating a chill block which constructs the agitator.

FIG. 6 shows a time table for a mass production system based on the use of the production apparatus.

FIG. 7 illustrates the temperature change of each of portions in a crucible during the operation of the production apparatus.

FIG. 8 shows an illustrative perspective view depicting the operation of the production apparatus.

FIG. 9 shows an illustrative perspective view depicting the operation of the production apparatus.

FIG. 10 shows an illustrative schematic perspective view depicting a production apparatus for carrying out a method for producing semisolidified metal according to a second embodiment of the present invention.

FIGS. 11A to 11F show steps illustrating the operation of the production apparatus.

FIG. 12 shows an illustrative schematic perspective view depicting a production apparatus for carrying out a method for producing semisolidified metal according to a third embodiment of the present invention.

FIGS. 13A to 13G show steps illustrating the operation of the production apparatus.

FIG. 14 illustrates a chill block having a cylindrical configuration.

FIG. 15 illustrates a chill block having a bottom-equipped cylindrical configuration.

FIG. 16 shows an illustrative schematic perspective view depicting a production apparatus for carrying out a method for producing semisolidified metal according to a fourth embodiment of the present invention.

FIG. 17 illustrates an agitator which constructs the production apparatus.

FIG. 18 shows an illustrative schematic perspective view depicting the agitator.

FIG. 19 shows an illustrative schematic perspective view depicting an agitator which constructs a production apparatus for carrying out a method for producing semisolidified metal according to a fifth embodiment of the present invention.

FIG. 20 shows an illustrative schematic perspective view depicting an agitator which constructs a production apparatus for carrying out a method for producing semisolidified metal according to a sixth embodiment of the present invention.

FIG. 21 illustrates a chill block designed to have an external shape of an elliptical configuration.

FIG. 22 illustrates a chill block designed to have an external shape of a composite elliptical configuration.

FIG. 23 illustrates a chill block designed to have an external shape of a chamfered rectangular configuration.

FIG. 24 illustrates a chill block designed to have an external shape of a hexagonal configuration.

FIG. 25 illustrates a chill block designed to have an external shape of a chamfered hexagonal configuration.

FIG. 26 shows an illustrative schematic perspective view depicting an apparatus for producing semisolidified metal according to a seventh embodiment of the present invention.

FIG. 27 illustrates an agitator which constructs the production apparatus.

FIG. 28 illustrates, in cross section, chill blocks which construct the agitator.

FIG. 29 shows an illustrative schematic perspective view depicting an apparatus for producing semisolidified metal according to an eighth embodiment of the present invention.

FIG. 30 illustrates a chill block which constructs an apparatus for producing semisolidified metal according to a ninth embodiment of the present invention.

FIG. 31 shows an illustrative schematic view, with partial cross section, depicting an apparatus for producing semisolidified metal according to a tenth embodiment of the present invention.

FIG. 32 illustrates a magnified view depicting a cooling member which constructs the production apparatus.

FIG. 33A illustrates a step of supplying molten metal to a crucible.

FIG. 33B illustrates a step of raising the crucible to immerse the cooling member in the molten metal.

FIG. 33C illustrates a step of supplying first liquid metal to the cooling member to cool and agitate the molten metal.

FIG. 33D illustrates a step of supplying second liquid metal to the cooling member after the semisolidified metal is produced.

#### BEST MODE FOR CARRYING OUT THE INVENTION

**[0020]** FIG. 1 shows an illustrative schematic perspective view depicting a production apparatus 10 for carrying out a method for producing semisolidified metal according to the first embodiment of the present invention, and FIG. 2 shows an illustrative plan view depicting the production apparatus 10.

**[0021]** The production apparatus 10 comprises a molten metal-holding furnace 14 for holding molten metal 12 which is composed of melted metal such as

aluminum, alloy thereof, magnesium, and alloy thereof; a molten metal-ladling robot 16 for ladling a predetermined amount (amount for one shot) of the molten metal 12 from the molten metal-holding furnace 14; a supply robot 26 for pouring the molten metal 12 ladled by the molten metal-ladling robot 16 into a predetermined heat-insulating crucible 18, and supplying semisolidified metal 20 formed into a desired slurry state in the crucible 18 to a slurry-introducing port 24 which communicates with an unillustrated cavity of a forming machine 22; and first to fourth agitators 28a to 28d each of which is arranged for the crucible 18 for cooling and agitating the molten metal 12 in the crucible 18.

**[0022]** As shown in FIGS. 1 and 3, the molten metal-ladling robot 16 includes an arm 32 which is provided swingably on a support pillar 30. A ladle 34 is installed tiltably to the forward end of the arm 32. The supply robot 26 is movable back and forth along a rail 36 which extends in a direction (direction of the arrow A) of arrangement of the first to fourth agitator 28a to 28d. The supply robot 26 is an articulated type robot, and it has, at its forward end, a gripping section 38 capable of holding the heat-insulating crucible 18.

**[0023]** The first agitator 28a includes a crucible holder 40 on which the crucible 18 is detachably arranged. As shown in FIG. 4, the crucible holder 40 is provided with a recess 42 for accommodating the crucible 18. A heater 44 is embedded at the inside of the crucible holder 40 so that the heater 44 circumscribes the crucible 18 arranged in the recess 42.

**[0024]** A chill block (cooling member) 46, which also has an agitating function, is detachably arranged with a driving mechanism 48 at a position over the crucible holder 40. The chill block 46 is made of, for example, a material such as copper and stainless steel which is not melted at the molten temperature of aluminum molten metal to be used as the molten metal 12. The external shape of the chill block 46 is designed to have a columnar configuration, with a draft sloped downwardly.

**[0025]** The chill block 46 is detachable with respect to a driving mechanism 48 by the aid of a coupler 49 made of ceramics. The driving mechanism 48 is moved upwardly and downwardly over the crucible holder 40, and it drives and rotates the chill block 46.

**[0026]** The second to fourth agitators 28b to 28d are constructed in the same manner as the first agitator 28a described above. The same constitutive components are designated by the same reference numerals, detailed explanation of which will be omitted.

**[0027]** Each of the chill blocks 46 is detachable with respect to each of the driving mechanisms 48 provided for the first to fourth agitators 28a to 28d. The chill block 46 is detached from the driving mechanism 48 every time when the molten metal 12 is agitated and cooled (for every one shot), and it is fed to a chill block-treating unit 50.

**[0028]** As shown in FIGS. 5A to 5E, the chill block-

treating unit 50 comprises a cooling tank 52 for cooling the chill block 46 disengaged from the driving mechanism 48 with a cooling medium such as cooling oil; an air blow means 54 for effecting air blow against the chill block 46 after the cooling to remove solidified matters of aluminum from the surface; a coating tank 56 for immersing the chill block 46 after the air blow in a coating liquid composed of a ceramic material; and a drying means 60 for drying the chill block 46 after the coating with a heater 58.

[0029] The operation of the production apparatus 10 constructed as described above will be explained below. FIG. 6 shows a time table for the mass production system based on the use of the production apparatus 10.

[0030] At first, the molten metal-ladling robot 16 is operated in a state in which the molten metal 12 is heated and maintained at about 650 °C in the molten metal-holding furnace 14. As shown in FIG. 3, the molten metal-ladling robot 16 is operated as follows. That is, the ladle 34 is inserted into the molten metal-holding furnace 14 in accordance with the action of the arm 32. The ladle 34 is inclined or tilted, so that the molten metal 12 in an amount of one shot is ladled by the ladle 34. The ladle 34, which has ladled the molten metal 12, is moved to a pouring position (see the position depicted by two-dot chain lines in FIG. 3). On the other hand, the supply robot 26, which holds the empty crucible 18, is arranged at the pouring position by the aid of the gripping section 38 (see FIG. 1).

[0031] In this situation, the ladle 34 is tilted, and the molten metal 12 in the amount of one shot is poured into the crucible 18 held by the supply robot 26. Subsequently, the supply robot 26 inserts the crucible 18 at a predetermined position of each of the first to fourth agitators 28a to 28d, for example, into the recess 42 of the crucible holder 40 which constitutes the first agitator 28a. The heater is operated in the crucible holder 40 to maintain a predetermined temperature beforehand. The molten metal 12 in the crucible 18 arranged in the recess 42 is prevented from being cooled all at once by the surroundings.

[0032] In the first agitator 28a, the chill block 46 is previously heated and maintained at about 100 °C in order to remove any moisture and stabilize the cooling condition. The chill block 46 is immersed in the molten metal 12 in the crucible 18 while being rotated in a predetermined direction at a relatively low speed by the aid of the driving mechanism 48. After that, the rotation speed of the chill block 46 is increased in the molten metal 12 in accordance with the action of the driving mechanism 48. Thus, the molten metal 12 is quickly agitated while being cooled.

[0033] After the chill block 46 agitates the molten metal 12 for a preset period of time or until a slurry supply signal is inputted, the chill block 46 is raised and withdrawn from the crucible 18 while being rotated. Accordingly, the semisolidified metal 20, which is main-

tained to have a constant temperature as a whole, is obtained in the heat-insulating crucible 18.

[0034] Changes occur as shown in FIG. 7 in the steps for producing the semisolidified metal 20 described above, concerning the atmosphere in the crucible 18, the temperature of the crucible 18, the center temperature of the molten metal 12, the end temperature of the molten metal 12, and the temperature of the chill block 46.

[0035] On the other hand, the supply robot 26 is moved, for example, corresponding to the fourth agitator 28d which possesses the semisolidified metal 20 cooled and agitated to give a desired slurry state, of the first to fourth agitators 28a to 28d. In the fourth agitator 28d, the driving mechanism 48 waits at an upward position, and the chill block 46 is removed. The supply robot 26 grips the crucible 18 which is arranged on the crucible holder 40 of the fourth agitator 28d, and it takes the crucible 18 out of the fourth agitator 28d (see FIG. 8).

[0036] The supply robot 26 is further operated such that the crucible 18, which is gripped by the gripping section 38, is arranged with respect to the slurry-introducing port 24 of the forming machine 22, and then the crucible 18 is inverted. Accordingly, the semisolidified metal 20 in the crucible 18 is allowed to fall so that it falls to be supplied to the slurry-introducing port 24 (see FIG. 9). In the forming machine 22, the forming process is performed with the semisolidified metal 20 to obtain a predetermined formed product.

[0037] The supply robot 26 moves the empty crucible 18 to the air blow position to apply the air blow treatment thereto. Accordingly, any aluminum, which remains in the heat-insulating crucible 18, is removed. Subsequently, the inside of the crucible 18 is subjected to coating with a ceramic material or the like, and then the crucible 18 is arranged at the pouring position.

[0038] In the first agitator 28a, the chill block 46, which is retracted upwardly after performing the cooling and the agitation for the molten metal 12, is disengaged from the driving mechanism 48, and it is transported to the chill block-treating unit 50 by the aid of a robot or the like (see FIG. 5A). In the chill block-treating unit 50, as shown in FIG. 5B, the chill block 46 is firstly immersed in the cooling tank 52 to perform the cooling treatment. After that, the air blow means 54 is used to remove aluminum solidified matters adhered to the surface of the chill block 46 (see FIG. 5C). Further, as shown in FIG. 5D, the chill block 46 is immersed in a coating liquid in the coating tank 56 to coat the surface thereof with a ceramic material, because of the following reason. That is, the surface of the chill block 46 is prevented from any reaction with the molten metal 12, and it is easy to remove aluminum solidified matters adhered to the surface of the chill block 46.

[0039] The chill block 46 after the coating treatment is subjected to the drying treatment in accordance with the action of the heater 58 which constitutes the drying means 60. The chill block 46 is heated to a predeter-

mined temperature (see FIG. 5E). After the drying, the chill block 46 is installed to the driving mechanism 48, and it is used again to perform the cooling and agitating operations for the new molten metal 12.

**[0040]** In the first embodiment of the present invention, the molten metal 12 in the crucible 18 is cooled by using the chill block 46 which is maintained at the temperature lower than the temperature of the molten metal 12. The chill block 46 is rotated to effect the agitation. Accordingly, no directivity occurs during the cooling of the molten metal 12. It is possible to obtain the semisolidified metal 20 formed into the slurry uniformly and reliably as a whole. It is possible to supply the semisolidified metal 20 to the slurry-introducing port 24 of the forming machine 22 without heating the semisolidified metal 20 again.

**[0041]** As a result, it is possible to always obtain the stable semisolidified metal 20 for every one shot. Further, it is unnecessary to provide any equipment such as the reheating apparatus. Accordingly, the effect can be obtained such that it is possible to produce the semisolidified metal 20 economically and efficiently. Further, the external shape of the chill block 46 is designed to have the columnar configuration. It is possible to effectively prevent the chill block 46 from being deteriorated by the molten metal 12 formed into the slurry. The chill block 46 has the draft which is sloped downwardly. Accordingly, it is possible to smoothly withdraw the chill block 46 from the semisolidified metal 20.

**[0042]** In the first embodiment, the air blow means 54 is used to remove the aluminum solidified matters adhered to the surface of the chill block 46. However, in place of the air blow means 54, it is possible to use, for example, a vibration-generating means and a sandblast means.

**[0043]** In the first embodiment, the molten metal-ladling robot 16 for ladling the molten metal in the amount of one shot is provided between the molten metal-holding furnace 14 and the supply robot 26. However, it is not necessarily indispensable to use the molten metal-ladling robot 16 provided that the apparatus is constructed such that the molten metal 12 in the amount of one shot is directly fed from the molten metal-holding furnace 14 to the crucible 18 held by the supply robot 26.

**[0044]** FIG. 10 shows an illustrative schematic perspective view depicting a production apparatus 70 for carrying out a method for producing semisolidified metal according to the second embodiment of the present invention.

**[0045]** The production apparatus 70 comprises divided type crucibles 80a, 80b; divided type crucible holders 82a, 82b for accommodating the crucibles 80a, 80b; a molten metal-feeding means 86 for feeding molten metal 84 into the crucibles 80a, 80b; an agitator 88 for cooling and agitating the molten metal 84 in the crucibles 80a, 80b; and a supply robot 92 for integrally holding the crucibles 80a, 80b to take them out of the

crucible holders 82a, 82b, and feeding semisolidified metal 90 to the forming machine 22.

**[0046]** The crucibles 80a, 80b are constructed by dividing a bottom-equipped cylinder into two in the diametral direction. A pair of hook-shaped projections 94a, 94b and a pair of grooves 96a, 96b are arranged linearly in the axial direction on the outer circumferences of the crucibles 80a, 80b respectively (see FIG. 11A). A heat-resistance packing 97 is interposed between joining surfaces of the crucibles 80a, 80b.

**[0047]** As shown in FIG. 11A, the crucible holders 82a, 82b are constructed by dividing a bottom-equipped cylinder into two in the diametral direction. The crucible holders 82a, 82b are swingably supported at supporting points 98a, 98b of their respective lower end angular portions with respect to an installation plane 99. Rods 102a, 102b, which extend from cylinders 100a, 100b, are connected to side portions of the crucible holders 82a, 82b, while the cylinders 100a, 100b are tiltable with respect to the installation plane 99. When the crucible holders 82a, 82b are closed, a recess 104 is integrally formed therein. Heaters 106a, 106b are embedded to circumscribe the recess 104.

**[0048]** As shown in FIG. 10, the molten metal-feeding means 86 is provided with a ladle 108 for ladling the molten metal 84 in an amount of one shot from the molten metal-holding furnace 14. The ladle 108 is constructed tiltable and movably between the ladling position for the molten metal 84 and the pouring position for the crucibles 80a, 80b.

**[0049]** The agitator 88 is provided with a chill block (cooling member) 110 which is made of, for example, stainless steel. The external shape of the chill block 110 is designed to have a columnar configuration. The chill block 110 is rotatable and movable upwardly and downwardly by the aid of an unillustrated driving mechanism. The chill block 110 is inserted rotatably into a lid member 112. The lid member 112 is movable upwardly and downwardly in an integrated manner together with the chill block 110. It is desirable that the lid member 112 is made of a material having no gas permeability. The surface, which makes contact with the molten metal 84, is designed to be a planar surface or to have a conical or pyramidal configuration protruding toward the molten metal 84 at its central portion.

**[0050]** The supply robot 92 is provided with a wrist section 114. An opening/closing mechanism 115 is installed to the wrist section 114. The opening/closing mechanism 115 has cylinders 116a, 116b which serve as forward/backward moving means. Ends of arm members 120a, 120b disposed vertically downwardly are secured to rods 118a, 118b which extend in mutually opposite directions from the cylinders 116a, 116b. The arm members 120a, 120b are provided with a pair of outer projections 122a, 122b which are inserted into and engaged with the respective projections 94a, 94b of the crucibles 80a, 80b, and a pair of inner projections 124a, 124b which are fitted to the grooves 96a, 96b of

the crucibles 80a, 80b.

[0051] A lid member 126, which is positioned under the opening/closing mechanism 115 and which is made of a heat-insulating material, is secured to the supply robot 92. The lid member 126 makes tight contact with the upper surfaces of the crucibles 80a, 80b to ensure the heat-insulating performance of the crucibles 80a, 80b when the crucibles 80a, 80b are held by the arm members 120a, 120b. The lid member 126 also functions to avoid any leakage of the semisolidified metal 90.

[0052] In the second embodiment constructed as described above, the crucibles 80a, 80b are firstly inserted between the crucible holders 82a, 82b in a state in which the crucible holders 82a, 82b are mutually open to stand on the supporting points 98a, 98b as shown in FIG. 11A. Subsequently, the cylinders 100a, 100b are operated to displace the rods 102a, 102b frontwardly respectively. Accordingly, the crucible holders 82a, 82b make swinging movement in directions to make approach to one another. Therefore, the crucibles 80a, 80b are accommodated in the recess 104 which is formed integrally between the crucible holders 82a, 82b. In this arrangement, the size of the recess 104 is designed to be slightly smaller than the external shape of the crucibles 80a, 80b. The crucibles 80a, 80b are held in a liquid-tight manner with each other with the heat-resistance packings 97 intervening therebetween in a state in which the crucible holders 82a, 82b are mutually closed.

[0053] Subsequently, as shown in FIG. 11B, the ladle 108, which constitutes the molten metal-feeding means 86, ladles the molten metal 84 in the amount of one shot, and the molten metal 84 is fed into the crucibles 80a, 80b. The crucibles 80a, 80b are heated and held at a predetermined temperature (for example, 280 °C) by the aid of the heaters 106a, 106b embedded in the crucible holders 82a, 82b. The molten metal 84, which is aluminum molten metal maintained at 650 °C to 700 °C, is fed into the crucibles 80a, 80b.

[0054] On the other hand, in the agitator 88, the chill block 110 is heated to 100 °C in order to remove, for example, moisture. As shown in Fig. 11C, the chill block 110 is moved downwardly from a position over the crucibles 80a, 80b while being rotated. Accordingly, the chill block 110 cools the molten metal 84 in the crucibles 80a, 80b, and it agitates the molten metal 84. More preferably, the chill block 110 is immersed in the molten metal 84 in the crucibles 80a, 80b while being rotated in a predetermined direction at a relatively low speed. After that, the rotation speed of the chill block 110 is increased in the molten metal 84. Accordingly, the chill block 110 quickly agitates the molten metal 84 while cooling the molten metal 84.

[0055] During this process, the lid member 112 is moved downwardly integrally with the chill block 110. The lid member 112 is arranged on the open upper end side of the crucibles 80a, 80b. Accordingly, the surface

of the molten metal 84 is not oxidized during the cooling and the agitation effected by the chill block 110. Further, it is possible to reliably avoid any contamination of air into the molten metal 84.

[0056] The cooling and the agitation are performed for a predetermined period of time to obtain the semisolidified metal 90 in a desired slurry state. After that, the chill block 110 is taken out of the crucibles 80a, 80b while being rotated. On the other hand, the supply robot 92 is arranged over the crucibles 80a, 80b. The supply robot 92 is operated such that the arm members 120a, 120b are moved downwardly by the aid of the wrist section 114 (see FIG. 11D). The respective outer projections 122a, 122b are fitted to the projections 94a, 94b of the crucibles 80a, 80b. The respective inner projections 124a, 124b are fitted to the grooves 96a, 96b of the crucibles 80a, 80b.

[0057] Subsequently, as shown in FIG. 11E, the crucible holders 82a, 82b make swinging movement in directions to make separation from each other in accordance with the action of the cylinders 100a, 100b. The crucibles 80a, 80b, which have been held by the recess 104, are taken out in a state of being held by the arm members 120a, 120b. The wrist section 114 is arranged at a position over the slurry-introducing port 24 of the forming machine 22. After that, the cylinder 116a, 116b, which construct the opening/closing mechanism 115, are operated to displace the rods 118a, 118b in directions to make separation from each other.

[0058] Therefore, the arm members 120a, 120b are displaced in directions to make separation from each other. The crucibles 80a, 80b, which are held by the arm members 120a, 120b, are released from each other. The semisolidified metal 90 is produced integrally in the crucibles 80a, 80b. When the crucibles 80a, 80b are open, then the semisolidified metal 90 falls, and it is supplied to the slurry-introducing port 24 (see FIG. 11F).

[0059] As described above, in the second embodiment, the molten metal 84 in the amount of one shot, which is fed into the crucibles 80a, 80b, are agitated in accordance with the rotating action of the chill block 110 while being cooled by the chill block 110. Accordingly, it is possible to obtain the semisolidified metal 90 in a satisfactory slurry state, which has no directivity of cooling and which is uniform as a whole. Further, the open ends of the crucibles 80a, 80b are closed by the lid member 112 during the cooling and the agitation effected by the chill block 110. Therefore, it is possible to effectively avoid any oxidation of the surface of the molten metal 84 and any contamination of air into the molten metal 84. Accordingly, such an effect is obtained that the semisolidified metal 90 having a high quality can be efficiently obtained.

[0060] The apparatus further includes the divided type crucibles 80a, 80b. The arm members 120a, 120b, which constitute the robot 92, are engaged with the crucibles 80a, 80b respectively so that the crucibles 80a,

80b may be opened and closed. Accordingly, the semi-solidified metal 90 is reliably allowed to fall, and it can be easily supplied to the slurry-introducing port 24 merely by moving the crucibles 80a, 80b in the directions to make separation from each other at the position over the slurry-introducing port 24.

**[0061]** Therefore, in the second embodiment, the entire amount of the semisolidified metal 90 can be reliably discharged from the crucibles 80a, 80b with the simple arrangement without being affected, for example, by the temperature of the semisolidified metal 90 in the crucibles 80a, 80b, the shape of the crucibles 80a, 80b, and the weight of the semisolidified metal 90. Accordingly, the supply weight of the semisolidified metal 90 is not dispersed, which would be otherwise caused by the occurrence of any remaining matter of the semisolidified metal 90 in the crucibles 80a, 80b. Further, such an effect is obtained that it is possible to effectively prevent the semisolidified metal 90 to be newly produced in the crucibles 80a, 80b from being badly affected.

**[0062]** FIG. 12 shows an illustrative schematic perspective view depicting a production apparatus 130 for carrying out a method for producing semisolidified metal according to the third embodiment of the present invention.

**[0063]** The production apparatus 130 comprises divided type crucibles 140a, 140b; divided type crucible holders 142a, 142b; a robot 144 for transporting the crucibles 140a, 140b; a molten metal-feeding means 148 for feeding molten metal 146 in an amount of one shot into the crucibles 140a, 140b; and an agitator 150 for cooling and agitating the molten metal 146 in the crucibles 140a, 140b.

**[0064]** A pair of projections 152a, 152b are formed to expand on outer circumferential portions of the crucibles 140a, 140b. The crucible holder 142a is connected to a rod 158 which extends from a cylinder 156, and it is movable back and forth in directions of the arrow by the aid of a pulley 160. The crucible holder 142b is fixed to an installation plane 161. When the crucible holders 142a, 142b are mutually closed, a recess 162 is integrally formed therein. Heaters 164a, 164b are embedded in the crucible holders 142a, 142b respectively (see FIG. 13A).

**[0065]** An opening/closing mechanism 166 is installed to the robot 144. Upper ends of arm members 172a, 172b are connected to rods 170a, 170b which extend from cylinders 168a, 168b for constructing the opening/closing mechanism 166. Fastening means 174a, 174b, which are used to make engagement with the projections 152a, 152b provided on the side surfaces of the crucibles 140a, 140b, are provided on lower end sides of the arm members 172a, 172b.

**[0066]** The molten metal-feeding means 148 is provided with a ladle 176. The agitator 150 is provided with a chill block 178 having a relatively small diameter. The chill block 178 is rotatable by the aid of a driving mechanism 180.

The driving mechanism 180 is installed to a movable base 182, and it is movable in the direction of the arrow (in the horizontal direction).

**[0067]** In the third embodiment constructed as described above, the operation is firstly performed as shown in FIG. 13A. That is, in a state in which the crucible holder 142a is separated from the crucible holder 142b, the crucibles 140a, 140b are gripped by the robot 144, and they are inserted into the crucible holders 142a, 142b. Subsequently, the crucible holder 142a is moved toward the crucible holder 142b to be mutually closed in accordance with the driving action of the cylinder 156. The crucibles 140a, 140b are accommodated and held in the recess 162 which is integrally formed therebetween (see FIG. 13B).

**[0068]** Further, as shown in FIG. 13C, the molten metal 146 in the amount of one shot is fed into the crucibles 140a, 140b by the aid of the ladle 176 which constitutes the molten metal-feeding means 148. After that, as shown in FIG. 13D, the agitator 150 is operated. In the agitator 150, the chill block 178, which is cooled at a predetermined temperature, is rotated by the aid of the driving mechanism 180 while being immersed in the molten metal 146. The movable base 182 is moved back and forth in the horizontal direction. Accordingly, the molten metal 146 in the crucibles 140a, 140b is cooled and agitated to obtain the semisolidified metal 184 having a desired slurry state.

**[0069]** Subsequently, as shown in FIG. 13E, the arm members 172a, 172b, which construct the robot 144, enter the inside of the crucible holders 142a, 142b to grip the crucibles 140a, 140b. After that, the crucible holder 142a is operated to be open in accordance with the action of the cylinder 156, while the robot 144 is moved upwardly (see FIG. 13F). The robot 144 arranges the crucibles 140a, 140b corresponding to the predetermined slurry-introducing port 24. When the arm members 172a, 172b make swinging movement in directions to make separation from each other in accordance with the action of the cylinders 168a, 168b, then the crucibles 140a, 140b mutually make swinging movement in opening directions, and thus the semisolidified metal 184 falls to be supplied to the slurry-introducing port 24 (see FIG. 13G).

**[0070]** Therefore, in the third embodiment, the same effect as that of the second embodiment is obtained by using the divided type crucibles 140a, 140b.

**[0071]** In the first to third embodiments, the chill blocks 46, 110, 178 are designed to have the columnar configuration. However, it is enough that at least the external shape has the columnar configuration. For example, a chill block 186 shown in FIG. 14 includes a cylindrical member 188, and an attachment plate 189 to which an end of the cylindrical member 188 is secured. A chill block 190 shown in FIG. 15 includes a bottom-equipped cylindrical member 192, and a shaft member 194 which is secured to an inner bottom portion 192a of the cylindrical member 192.



**[0072]** FIG. 16 shows an illustrative schematic perspective view depicting a production apparatus 200 for carrying out a method for producing semisolidified metal according to the fourth embodiment of the present invention. The same constitutive components as those of the production apparatus 70 according to the second embodiment shown in FIG. 10 are designated by the same reference numerals, detailed explanation of which will be omitted.

**[0073]** The production apparatus 200 is provided with an agitator 202. As shown in FIGS. 16 and 17, a chill block (cooling member) 204, which constructs the agitator 202, is detachably arranged with respect to a rotary section 206 with a coupler 208 made of ceramics intervening therebetween, at a position over crucible holders 82a, 82b. The chill block 204 is composed of, for example, a material such as copper and stainless steel which is not melted at a melting temperature of aluminum molten metal to be used as the molten metal 84. The external shape of the chill block 204 is designed to have a quadratic prism-shaped configuration, with a draft formed downwardly.

**[0074]** The rotary section 206 rotates and drives the chill block 204. The rotary section 206 is constructed to be movable upwardly and downwardly in an integrated manner together with the chill block 204 by the aid of a moving section 210, and it is moved along a spiral configuration in the horizontal direction (see FIG. 18). That is, the moving section 210 has two functions of an elevator means and a spiral movable means. A driving mechanism is constructed by the rotary section 206 and the moving section 210.

**[0075]** As shown in FIG. 18, in the production apparatus 200 according to the fourth embodiment constructed as described above, the molten metal 84 in the crucibles 80a, 80b is cooled by the chill block 204 which is maintained at a temperature lower than the temperature of the molten metal 84. The molten metal 84 is agitated by moving the chill block 204 in the spiral configuration in the horizontal direction along the shape of the crucibles 80a, 80b while rotating the chill block 204. Accordingly, no directivity occurs during the cooling of the molten metal 84 in the crucibles 80a, 80b. It is possible to quickly obtain the desired semisolidified metal 90 formed into the slurry uniformly and reliably as a whole. Therefore, it is unnecessary to reheat the semisolidified metal 90. The semisolidified metal 90 can be directly supplied to the slurry-introducing port 24 of the forming machine 22.

**[0076]** Accordingly, the following effects are obtained. That is, it is possible to always obtain the stable semisolidified metal 90 for every one shot. Further, it is unnecessary to provide the equipment such as the reheating unit, and it is possible to produce the semisolidified metal 90 economically and efficiently. The external shape of the chill block 204 is designed to have the quadratic prism-shaped configuration. Therefore, it is possible to reliably agitate the molten metal 84. The chill

block 204 has the draft formed downwardly. Thus, the chill block 204 can be smoothly withdrawn from the semisolidified metal 90.

**[0077]** FIG. 19 shows an illustrative schematic perspective view depicting an agitator 290 which constructs a production apparatus for carrying out a method for producing semisolidified metal according to the fifth embodiment of the present invention.

**[0078]** The agitator 290 is provided with a pair of chill blocks (cooling members) 296a, 296b for cooling and agitating molten metal 294 in divided type crucibles 292a, 292b. The chill blocks 296a, 296b are arranged detachably with respect to rotary sections 298a, 298b with couplers 300a, 300b made of ceramics intervening therebetween. The chill blocks 296a, 296b are made of, for example, copper or stainless steel, in the same manner as the chill block 204. The chill blocks 296a, 296b are designed to have a quadratic prism-shaped external shape, and they have a draft formed downwardly.

**[0079]** The rotary sections 298a, 298b rotate and drive the chill blocks 296a, 296b. On the other hand, the rotary sections 298a, 298b are movable upwardly and downwardly in an integrated manner together with the chill blocks 296a, 296b by the aid of a moving section 302, and they make reciprocating movement in the horizontal direction along the longitudinal direction (direction of the arrow A) of the crucibles 292a, 292b. That is, the moving section 302 has two functions of an elevator means and a horizontally moving means.

**[0080]** The crucibles 292a, 292b are designed to have a rectangular configuration in a state of making tight contact with each other. A heat-resistant packing 304 is interposed between their joining surfaces. The crucibles 292a, 292b are arranged on unillustrated divided type crucible holders. An integrated type crucible may be adopted in place of the divided type crucibles 292a, 292b.

**[0081]** In the fifth embodiment constructed as described above, the molten metal 294 in an amount of one shot is firstly fed into the inside of the crucibles 292a, 292b which are allowed to make tight contact with each other. After that, the chill blocks 296a, 296b are arranged at positions over the crucibles 292a, 292b by the aid of the moving section 302. Subsequently, the chill blocks 296a, 296b are moved downwardly while being rotated in accordance with the action of the rotary sections 298a, 298b.

**[0082]** The chill blocks 296a, 296b are moved in a reciprocating manner in the horizontal direction in accordance with the action of the moving section 302, after the chill blocks 296a, 296b are immersed in the molten metal 294 in the crucibles 292a, 292b, or simultaneously with the rotary driving. Accordingly, the chill blocks 296a, 296b cool the molten metal 294 in the crucibles 292a, 292b, and they agitate the molten metal 294 along the shape of the crucibles 292a, 292b.

**[0083]** As described above, in the fifth embodiment, the chill blocks 296a, 296b make the reciprocating

movement along the longitudinal direction (direction of the arrow A) of the crucibles 292a, 292b while being rotated. Accordingly, the molten metal 294 can be agitated reliably and effectively over the entire interior of the crucibles 292a, 292b. Therefore, the same effects as those obtained in the fourth embodiment are obtained, for example, such that it is possible to obtain the desired semisolidified metal 90 in the satisfactory slurry state which is uniform as a whole and which has no directivity of cooling, in the crucibles 292a, 292b.

**[0084]** FIG. 20 shows an illustrative schematic perspective view depicting an agitator 320 which constructs a production apparatus for carrying out a method for producing semisolidified metal according to the sixth embodiment of the present invention.

**[0085]** The agitator 320 is provided with a chill block (cooling member) 326 for cooling and agitating molten metal 324 in divided type crucibles 322a, 322b. The chill block 326 is arranged detachably with respect to a rotary section 328 with a coupler 330 made of ceramics intervening therebetween. The chill block 326 is made of, for example, copper or stainless steel, in the same manner as the chill block 204 described above. The chill block 326 is designed to have a quadratic prism-shaped external shape, and it has a draft formed downwardly.

**[0086]** A rotary section 328 rotates and drives the chill block 326. On the other hand, the rotary section 328 is movable upwardly and downwardly in an integrated manner together with the chill block 326 by the aid of a moving section 332. That is, the moving section 332 has a function to serve as a vertically moving means for making reciprocating movement of the chill block 326 in the longitudinal direction (direction of the arrow B) of the crucibles 322a, 322b.

**[0087]** The crucibles 322a, 322b are designed to have a cylindrical configuration in a state of making tight contact with each other. A heat-resistant packing 334 is interposed between their joining surfaces. The crucibles 322a, 322b are arranged on unillustrated divided type crucible holders. An integrated type crucible may be adopted in place of the divided type crucibles 322a, 322b.

**[0088]** In the sixth embodiment constructed as described above, the molten metal 324 in an amount of one shot is firstly fed into the inside of the crucibles 322a, 322b which are allowed to make tight contact with each other. After that, the chill block 326 is arranged at a position over the crucibles 322a, 322b by the aid of the moving mechanism 332.

**[0089]** Subsequently, the chill block 326 is moved downwardly by the aid of the moving section 332 while being rotated in accordance with the action of the rotary section 328. The chill block 326 is immersed in the molten metal 324 in the crucibles 322a, 322b, and then it makes reciprocating movement in the vertical direction in accordance with the action of the moving section 332. Accordingly, the chill block 326 cools the molten metal 324 in the crucibles 322a, 322b, and it agitates the mol-

ten metal 324 along the shape of the crucibles 322a, 322b.

**[0090]** As described above, in the sixth embodiment, the chill block 326 makes the reciprocating movement in the longitudinal direction (direction of the arrow B) of the crucibles 322a, 322b while being rotated. Accordingly, the molten metal 324 can be agitated reliably and effectively over the entire interior of the crucibles 322a, 322b. Therefore, the same effects as those obtained in the fourth and fifth embodiments are obtained, for example, such that it is possible to obtain the desired semisolidified metal 90 in the satisfactory slurry state which is uniform as a whole and which has no directivity of cooling.

**[0091]** In the fourth to sixth embodiments, each of the chill blocks 204, 296a, 296b, 326 is designed to have the rectangular configuration. However, there is no limitation thereto. For example, it is also allowable to use a chill block 340 designed to have an external shape of an elliptical configuration (see FIG. 21), a chill block 342 designed to have an external shape of a composite elliptical configuration (see FIG. 22), a chill block 344 designed to have an external shape of a chamfered rectangular configuration (see FIG. 23), a chill block 346 designed to have an external shape of a hexagonal configuration (see FIG. 24), and a chill block 346 designed to have an external shape of chamfered hexagonal configuration (see FIG. 25).

**[0092]** FIG. 26 shows an illustrative schematic perspective view depicting an apparatus 400 for producing semisolidified metal according to the seventh embodiment of the present invention. The same constitutive components as those of the production apparatus 200 according to the fourth embodiment shown in FIG. 16 are designated by the same reference numerals, detailed explanation of which will be omitted.

**[0093]** The production apparatus 400 is provided with an agitator 402. A plurality of chill blocks (cooling members) 406a to 406d, which construct the agitator 402, are detachably connected to a rotary section 206 with a coupler 208 made of ceramics intervening therebetween, at a position over crucible holders 82a, 82b. The chill blocks 406a to 406d are composed of, for example, a material such as copper and stainless steel which is not melted at a melting temperature of aluminum molten metal to be used as the molten metal 84. As shown in FIGS. 26 to 28, the external shape of the entire chill blocks 406a to 406d is designed to have a quadratic prism-shaped configuration, with a draft formed downwardly.

**[0094]** As shown in FIG. 28, through-holes 408a to 408d are formed at respective central portions of the chill blocks 406a to 406d. An arbitrary number of the chill blocks 406a to 406d can be held in an integrated manner with respect to the rotary section 206 by the aid of a fixing means 412. The fixing means 412 includes a screw shaft (shaft member) 414 for being integrally inserted into the through-holes 408a to 408d of the

stacked chill blocks 406a to 406d, a nut member (fix-  
ture) 416 for being screwed on the lower end of the  
screw shaft 414, and a support plate 415 for supporting  
the chill blocks 406a to 406d. The upper end of the  
screw shaft 414 can be detachably connected to the  
coupler 208.

[0095] In the case of the production apparatus 400  
constructed as described above, when the weight of the  
molten metal 84 in the amount of one shot is changed  
depending on the change of the part to be formed, the  
number of chill blocks 406a to 406d installed to the  
rotary section 206 is increased or decreased. Specifi-  
cally, when the weight of the molten metal 84 in the  
amount of one shot is decreased, the chill blocks 406a  
to 406d are decreased, for example, to the chill blocks  
406a to 406c. On the other hand, when the weight of the  
molten metal 84 in the amount of one shot is increased,  
a predetermined number of chill blocks (not shown) may  
be stacked on the chill blocks 406a to 406d.

[0096] As described above, in the seventh embodi-  
ment, the molten metal 84 in the crucibles 80a, 80b is  
cooled with the predetermined number of chill blocks  
406a to 406d, and the chill blocks 406a to 406d are  
rotated in an integrated manner by the aid of the rotary  
section 206 to agitate the molten metal 84. Accordingly,  
the following effects are obtained. That is, no directivity  
occurs during the cooling of the molten metal 84 in the  
crucibles 80a, 80b. It is possible to extremely quickly  
and efficiently obtain the desired semisolidified metal 22  
formed into the slurry uniformly and reliably as a whole.

[0097] Further, when the weight of the molten metal  
84 in the amount of one shot is changed, it is enough  
that the number of chill blocks 406a to 406d is increased  
or decreased depending on the weight of the molten  
metal 84. It is possible to efficiently and highly accu-  
rately produce the semisolidified metal 90 for forming a  
variety of different parts. Accordingly, the following  
advantages are obtained. That is, it is unnecessary to  
prepare any exclusive cooling means corresponding to  
the change of the weight of the molten metal 84. It is  
possible to effectively reduce the equipment cost.

[0098] FIG. 29 shows an illustrative schematic per-  
spective view depicting an apparatus 490 for producing  
semisolidified metal according to the eighth embodi-  
ment of the present invention. The same constitutive  
components as those of the production apparatus 400  
according to the seventh embodiment are designated  
by the same reference numerals, detailed explanation of  
which will be omitted.

[0099] The production apparatus 490 includes a  
plurality of chill blocks (cooling members) 492a to 492d  
which also possess the agitating function. The chill  
blocks 492a to 492d are detachably arranged with  
respect to the driving mechanism 494 with a coupler  
496 made of ceramics intervening therebetween. The  
chill blocks 492a to 492d are made of, for example, cop-  
per or stainless steel, and their upper ends are inte-  
grated into one unit with a connecting section 498. The

connecting section 498 is detachable with respect to the  
coupler 496. The external shape of each of the chill  
blocks 492a to 492d is designed to have a columnar  
configuration, and each of the chill blocks 492a to 492d  
has a draft formed downwardly.

[0100] In the eighth embodiment constructed as  
described above, the molten metal 84 in an amount of  
one shot is fed into the crucibles 80a, 80b. After that, the  
chill blocks 492a to 492d are moved downwardly while  
being rotated by the aid of the driving mechanism 494,  
and they are immersed in the molten metal 84 in the  
crucibles 80a, 80b. Accordingly, the molten metal 84 in  
the crucibles 80a, 80b is cooled and agitated to obtain  
the semisolidified metal 90 having a desired slurry state.

[0101] Accordingly, in the eighth embodiment, the  
four chill blocks 492a to 492d are operated in an inte-  
grated manner to agitate the molten metal 84 while  
cooling the molten metal 84 in the crucibles 80a, 80b.  
Therefore, even when the weight of the molten metal 84  
is especially large, an effect is obtained such that the  
desired semisolidified metal 90 can be obtained effi-  
ciently and quickly.

[0102] FIG. 30 illustrates a chill block 500 which  
constructs an apparatus for producing semisolidified  
metal according to the ninth embodiment of the present  
invention.

[0103] The chill block 500 is provided with a plurality  
of rib sections 504a to 504i which are integrally formed  
on the outer circumference of a columnar section 502  
while being separated from each other by predeter-  
mined spacing distances in the axial direction. There-  
fore, in the ninth embodiment, when the chill block 500  
is rotated in the molten metal 84, the molten metal 84 is  
cooled and agitated quickly and smoothly by the aid of  
the plurality of rib sections 504a to 504i. Thus, it is pos-  
sible to obtain the same effects as those obtained in the  
seventh and eighth embodiments.

[0104] FIG. 31 shows an illustrative schematic view,  
with partial cross section, depicting an apparatus 510  
for producing semisolidified metal according to the tenth  
embodiment of the present invention.

[0105] The production apparatus 510 comprises a  
heat-insulating crucible 514 for holding molten metal  
512 composed of melted metal in a predetermined  
amount (amount of one shot); a coil-shaped cooling  
member 516 for cooling the molten metal 512 in the cru-  
cible 514 to a predetermined temperature; a cooling  
mechanism 520 for supplying, to the inside of the cool-  
ing member 516, first liquid metal 518 as a cooling  
medium maintained at a temperature which is not more  
than the temperature of the molten metal 512; and an  
electromagnetic agitation mechanism (driving mecha-  
nism) 522 for agitating the molten metal 512 by the aid  
of the cooling member 516.

[0106] The crucible 514 is made of, for example, sil-  
icon nitride. The crucible 514 is arranged on an elevator  
base 524. A heating heater 526 is installed to the outer  
circumference of the crucible 514. The elevator base

524 is movable upwardly and downwardly by the aid of an unillustrated driving means, and it is designed to be rotatable, if necessary. A coil section 528, which constructs the electromagnetic agitation mechanism 522, is arranged to surround the crucible 514 in the vicinity of the elevator base 524.

**[0107]** The cooling mechanism 520 includes a first supply means 530 for supplying first liquid metal 518 into the cooling member 516 in order to cool the molten metal 512 to a predetermined temperature, and a second supply means 534 for supplying, into the cooling member 516, second liquid metal 532 which is a heating medium having a temperature higher than a liquefying temperature of solidified matters in order to remove the solidified matters adhered to the surface of the cooling member 516. The molten metal 512 is melted metal composed of, for example, aluminum, alloy thereof, magnesium, or alloy thereof. The first and second liquid metals 518, 532 are stannum or stannum alloy.

**[0108]** The first supply means 530 includes a first storage tank 536 for storing the first liquid metal 518; a first heating furnace (first heating section) 538 for keeping the temperature of the first liquid metal 518 in the first storage tank 536; a heat exchanger 540 for cooling the first liquid metal 518 by performing heat exchange with respect to the first liquid metal 518; and a first circulating passage 542 for circulating the first liquid metal 518 through the inside of the cooling member 516.

**[0109]** The heat exchanger 540 is provided with a heat exchange coil 544 for supplying cooling water thereinto. The heat exchange coil 44 is immersed in the first liquid metal 518 in the first storage tank 536. The first heating furnace 538 is arranged to circumscribe the first storage tank 536. The first circulating passage 542 is composed of a pipe made of SUS. An inlet end 542a thereof is connected to a lower end side of the first storage tank 536. An outlet end 542b thereof is immersed at a predetermined height position in the first liquid metal 518 at an upward portion of the first storage tank 536. As shown in FIG. 32, the first circulating passage 542 constitutes a part of the cooling member 516. A first electromagnetic pump 546 is arranged on the side of the end 542a (see FIG. 31).

**[0110]** The second supply means 534 includes a second storage tank 548 for storing the cooling member 532; a second heating furnace (second heating section) 550 for heating the cooling member 532 in the second storage tank 548; and a second circulating passage 552 for circulating the cooling member 532 through the inside of the cooling member 516.

**[0111]** The second heating furnace 550 is arranged to circumscribe the second storage tank 548. The second circulating passage 552 has its inlet end 552a which is joined to the lower side of the second storage tank 548, and its outlet end 552b which is immersed at a predetermined position in the second liquid metal 532 at an upper portion of the second storage tank 548. A second electromagnetic pump 554 is provided for the

second circulating passage 552 in the vicinity of the side of the end 552a. The second circulating passage 552 is joined with the first circulating passage 542 at its intermediate portion to constitute a part of the cooling member 516 (see FIG. 32).

**[0112]** A first thermocouple (first detecting means) 558 for measuring the temperature of the molten metal is installed at the joined portion of the first and second circulating passages 542, 552 by the aid of a support member 556. The first thermocouple 558 detects the temperature of the molten metal 512 in the crucible 514. A second thermocouple (second detecting means) 560 for detecting the temperature of the first liquid metal 518 is arranged for the first storage tank 536 which constructs the first supply means 530. On the other hand, a third thermocouple (third detecting means) 562 for detecting the temperature of the second liquid metal 532 is arranged for the second storage tank 548 which constructs the second supply means 534.

**[0113]** Explanation will be made below for the operation of the production apparatus 510 according to the tenth embodiment constructed as described above.

**[0114]** At first, the operation is performed as shown in FIG. 33A. That is, for example, the molten metal 512 of aluminum alloy (AC2B), which is used as a material for the molten metal, is held at a temperature of 650 °C in an unillustrated molten metal-holding furnace. A feeder 564 ladles the molten metal 512 in an amount of one shot, for example, in an amount of 20 kg to be fed to the crucible 514. The heater 526 is installed to the crucible 514. The temperature of the molten metal 512 in the crucible 514 is maintained to be constant by the aid of the heater 526.

**[0115]** Subsequently, as shown in FIG. 33B, the elevator base 524, on which the crucible 514 is placed, is moved upwardly. The cooling member 516 is immersed in the molten metal 512 in the crucible 514. The cooling member 516 is a pipe made of SUS having an inner diameter of 20 mm, which is constructed to have a coil-shaped configuration with an entire length of 700 mm.

**[0116]** On the other hand, in the cooling mechanism 520, as shown in FIG. 31, the first liquid metal 518 is maintained at 250 °C, and it is stored in an amount of 100 liters in the first storage tank 536 which constitutes the first supply means 530. The second liquid metal 532 is maintained at 600 °C, and it is stored in an amount of 40 liters in the second storage tank 548 which constitutes the second supply means 534. The temperatures of the first and second liquid metals 518, 532 are detected by the second and third thermocouples 560, 562 respectively. The heat exchanger 540 and the first heating furnace 538 are operated on the basis of the result of the detection performed by the second thermocouple 560. Thus, the temperature of the first liquid metal 518 is maintained to be constant. On the other hand, the second heating furnace 550 is operated on the basis of the result of the detection performed by the

third thermocouple 562. Thus, the temperature of the second liquid metal 532 is maintained to be constant.

[0117] The first electromagnetic pump 546 is operated so that the first liquid metal 518 in the first storage tank 536 is introduced into the inside of the cooling member 516 via the first circulating passage 542 at a flow rate of 20 liters/minute. After that, the first liquid metal 518 is returned from the end 542b to the inside of the first storage tank 536 (see FIG. 33C). Accordingly, the molten metal 512 in the crucible 514 is cooled by the aid of the cooling member 516 in which the first liquid metal 518 having the relatively low temperature is circulated through the inside. During this process, the coil section 528, which constitutes the electromagnetic agitation mechanism 522, is operated to agitate the molten metal 512 in the crucible 514.

[0118] The temperature of the molten metal 512 in the crucible 514 is detected by the first thermocouple 558. The cooling and the agitation are performed for the molten metal 512 until the detected temperature arrives at the preset semisolidification temperature. Therefore, the semisolidified metal 566, which has no directivity of cooling and which is formed into the slurry uniformly and successfully as a whole, is produced in the crucible 514 (see FIGS. 31 and 33C).

[0119] Subsequently, the operation of the first electromagnetic pump 546 is stopped, and the second electromagnetic pump 554 is operated. Accordingly, as shown in FIG. 33D, the liquid metal 532 in the second storage tank 548 is supplied to the inside of the cooling member 516 via the second circulating passage 552 at a flow rate of 20 liters/minute. The second liquid metal 532 is held at a temperature higher than the liquefaction temperature of the aluminum alloy used for the molten metal 512. Even when aluminum solidified matters adhere to the surface of the cooling member 516, the aluminum solidified matters can be dissolved again to reliably remove them. After that, the operation of the second electromagnetic pump 554 is stopped, and the elevator base 524 is moved downwardly to separate the crucible 514 from the cooling member 516.

[0120] Accordingly, the desired semisolidified metal 566 is obtained in the crucible 514. During this process, the first and second liquid metals 518, 532 are supplied to the cooling member 516 at the flow rate of 20 liters/minute by the aid of the first and second electromagnetic pumps 546, 554. Therefore, the molten metal 512 in the crucible 514 is cooled from 650 °C to the slurry temperature of 570 °C for about 1 minute. On the other hand, it is possible to effectively prevent the surface of the cooling member 516 from adhesion of aluminum solidified matters.

[0121] In the tenth embodiment, the first liquid metal 518, which is maintained at the predetermined cooling temperature, is supplied in the circulating manner to the inside of the cooling member 516 to cool the molten metal 512 in the state in which the cooling member 516 is immersed in the molten metal 512 in the cru-

cible 514. Further, the electromagnetic agitation mechanism 522 is operated to agitate the molten metal 512. Accordingly, no directivity occurs during the cooling of the molten metal 512. It is possible to obtain the semisolidified metal 566 formed into the slurry uniformly and reliably as a whole.

[0122] The first and second thermocouples 558, 560 are used to detect the temperatures of the molten metal 512 and the first liquid metal 518 so that the temperature of the first liquid metal 518 is managed. Accordingly, it is unnecessary to reheat the semisolidified metal 566. Such an effect is obtained that the semisolidified metal 566 having a high quality can be efficiently obtained. Especially, it is advantageous that the temperature of the semisolidified metal 566 is managed easily and correctly, and the cooling speed for the molten metal 512 is improved so that the semisolidified metal 566 may be quickly produced all at once.

[0123] The tenth embodiment is provided with the second supply means 534 for supplying, to the inside of the cooling member 516, the second liquid metal 532 having the temperature higher than the liquefaction temperature of the molten metal material (for example, aluminum alloy) after the semisolidified metal 566 is produced. That is, it is feared that the aluminum solidified matters formed by the solidification of the molten metal 512 adhere to the surface of the cooling member 516 after performing the cooling and the agitation for the molten metal 512, resulting in formation of any solidified layer. If the solidified layer has a thick wall thickness, then it is feared that the aluminum solidified matters are oxidized to cause contamination into the molten metal 512 in the crucible 514 upon the next time shot, or the aluminum solidified matters cause the change of the cooling condition of the molten metal 512 and the dispersion of the amount of the molten metal.

[0124] In the tenth embodiment, the second liquid metal 532 having the relatively high temperature is supplied to the second circulating passage 552. Therefore, the aluminum solidified matters, which adhere to the surface of the cooling member 516, are dissolved again, and they are reliably removed from the surface. Accordingly, it is possible to efficiently obtain the semisolidified metal 566 having the high quality, and it is possible to stabilize the cooling condition.

[0125] In the tenth embodiment, the cooling member 516 is designed to have the coil-shaped configuration in which the first and second circulating passages 542, 552 are joined to one another in the integrated manner. However, the cooling member 516 may be designed to have various configurations such as a plate-shaped configuration, for example, corresponding to the volume and the shape of the crucible 514. That is, the cooling member 516 may be designed to have an optimum configuration so that the surface area is increased.

[0126] The electromagnetic agitation mechanism 522 is used to agitate the molten metal 512. However, in

place thereof, it is possible to adopt a mechanical agitation structure. For example, the molten metal 512 may be agitated by rotating the crucible 514 itself, or by moving the crucible 514 in the horizontal direction together with the rotation of the crucible 514. Further, the following arrangement is also available. That is, the cooling member 516 itself may be rotated, or it may be designed to be movable in the horizontal direction.

#### INDUSTRIAL APPLICABILITY

**[0127]** As described above, in the present invention, the molten metal, which is supplied to the heat-insulating crucible, is agitated while being cooled by the aid of the cooling member. Therefore, the molten metal is formed into the slurry in the crucible uniformly and reliably as a whole. It is possible to easily and efficiently obtain the desired semisolidified metal having no directivity of cooling. Further, it is unnecessary to reheat the semisolidified metal. It is possible to reliably avoid the expensive equipment cost.

**[0128]** In the present invention, the molten metal in the crucible is cooled by the aid of the cooling member, and the molten metal is agitated by moving the cooling member along the shape of the crucible. Accordingly, the molten metal is formed into the slurry in the heat-insulating crucible uniformly and reliably as a whole. It is possible to easily and efficiently obtain the desired semisolidified metal having no directivity of cooling.

**[0129]** In the present invention, the molten metal in the crucible is cooled and agitated by the aid of the plurality of cooling members. Therefore, the directivity of cooling is excluded to be as less as possible, and it is possible to quickly and efficiently produce the desired semisolidified metal formed into the slurry uniformly and reliably as a whole.

**[0130]** In the present invention, the cooling member is immersed in the molten metal in the heat-insulating crucible. The molten metal is agitated in the state in which the cooling medium is supplied to the inside of the cooling member. Accordingly, no directivity occurs during the cooling of the molten metal, and it is possible to form the slurry of the molten metal quickly and reliably. Further, the desired semisolidified metal can be obtained efficiently and highly accurately by managing the temperature of the cooling medium.

**[0131]** In the present invention, the molten metal, which is contained in the divided type heat-insulating crucibles, is cooled and agitated by the aid of the cooling member to produce the semisolidified metal. After that, the heat-insulating crucibles are subjected to the opening/closing operation by the aid of the opening/closing mechanism. Accordingly, the semisolidified metal in the heat-insulating crucibles falls from the heat-insulating crucibles due to its own weight, and it is discharged therefrom.

Accordingly, the directivity of cooling is excluded to be as less as possible, and it is possible to obtain the

desired semisolidified metal formed into the slurry uniformly and reliably as a whole. Further, it is possible to discharge the semi-solidified metal from the heat-insulating crucibles smoothly and reliably by using the simple structure.

#### Claims

1. A method for producing semisolidified metal, comprising the steps of:

supplying a predetermined amount of molten metal to a heat-insulating crucible;  
cooling said molten metal in said heat-insulating crucible by the aid of a cooling member cooled to a predetermined temperature which is not more than a temperature of said molten metal, and agitating said molten metal; and completing said agitation step after agitating said molten metal to give a predetermined slurry state, and separating said cooling member from said heat-insulating crucible.

2. A method for producing semisolidified metal, comprising the steps of:

supplying a predetermined amount of molten metal to a heat-insulating crucible;  
cooling said molten metal in said heat-insulating crucible by the aid of a cooling member cooled to a predetermined temperature which is not more than a temperature of said molten metal, and agitating said molten metal by moving said cooling member in a horizontal direction and/or in a vertical direction while rotating said cooling member; and completing said agitation step after agitating said molten metal to give a predetermined slurry state, and separating said cooling member from said heat-insulating crucible.

3. The method for producing said semisolidified metal according to claim 1 or 2, further comprising the steps of:

agitating said molten metal in said heat-insulating crucible by rotating said cooling member in said heat-insulating crucible;  
removing solidified matters adhered to a surface of said cooling member after separating said cooling member from said heat-insulating crucible; and applying a drying treatment to said cooling member after removing said solidified matter.

4. The method for producing said semisolidified metal according to claim 3, wherein said cooling member is coated with a ceramic material after removing

said solidified matters.

5. The method for producing said semisolidified metal according to any one of claims 1 to 4, wherein an external shape of said cooling member is set to have a columnar configuration with a draft formed downwardly. 5
6. The method for producing said semisolidified metal according to any one of claims 1 to 4, wherein an external shape of said cooling member is set to have a non-columnar configuration with a draft formed downwardly. 10
7. The method for producing said semisolidified metal according to claim 1 or 2, wherein said cooling member is inserted into said heat-insulating crucible, and an open end of said heat-insulating crucible is closed by a lid member. 15
8. The method for producing said semisolidified metal according to claim 1 or 2, wherein a plurality of cooling members are provided. 20
9. An apparatus for producing semisolidified metal, comprising: 25
  - a heat-insulating crucible for holding predetermined molten metal;
  - a cooling member for cooling said molten metal in said heat-insulating crucible to a predetermined temperature; and
  - a driving mechanism for agitating said molten metal by rotating said cooling member. 30
10. The apparatus for producing said semisolidified metal according to claim 9, wherein an external shape of said cooling member is set to have a columnar configuration with a draft formed downwardly. 40
11. An apparatus for producing semisolidified metal, comprising: 45
  - a heat-insulating crucible for holding a predetermined amount of molten metal;
  - a cooling member for cooling said molten metal in said heat-insulating crucible to a predetermined temperature; and
  - a driving mechanism for agitating said molten metal by moving said cooling member in a horizontal direction and/or in a vertical direction while rotating said cooling member. 50
12. The apparatus for producing said semisolidified metal according to claim 11, wherein said driving mechanism includes a horizontal moving means for making reciprocating movement of said cooling 55

member in said horizontal direction.

13. The apparatus for producing said semisolidified metal according to claim 11, wherein said driving mechanism includes a spiral moving means for making spiral movement of said cooling member in said horizontal direction.
14. The apparatus for producing said semisolidified metal according to claim 11, wherein said driving mechanism includes a vertical moving means for making reciprocating movement of said cooling member in said vertical direction.
15. The apparatus for producing said semisolidified metal according to claim 11, wherein an external shape of said cooling member is set to have a non-columnar configuration with a draft formed downwardly.
16. An apparatus for producing semisolidified metal, comprising:
  - a heat-insulating crucible for holding a predetermined amount of molten metal;
  - a plurality of cooling members for cooling said molten metal in said heat-insulating crucible to a predetermined temperature; and
  - a driving mechanism for integrally driving said plurality of cooling members to effect agitation in said molten metal, said plurality of cooling members being detachable with respect to said driving mechanism.
17. The apparatus for producing said semisolidified metal according to claim 16, wherein said plurality of cooling members are capable of being integrally held by said driving mechanism by the aid of a fixing means in a state in which an arbitrary number of said plurality of cooling members are stacked with each other. 35
18. The apparatus for producing said semisolidified metal according to claim 17, wherein said fixing means includes:
  - a shaft member for being integrally inserted into said plurality of cooling members; and
  - a fixture for being screwed on an end of said shaft member. 40
19. The apparatus for producing said semisolidified metal according to claim 16, wherein said plurality of cooling members are integrated into one unit with a connecting section, and said connecting section is connectable to said driving mechanism via a coupler. 45

20. An apparatus for producing semisolidified metal, comprising:

a heat-insulating crucible for holding a predetermined amount of molten metal; 5  
 a cooling member for cooling said molten metal in said heat-insulating crucible to a predetermined temperature;  
 a cooling mechanism for supplying, into said cooling member, a cooling medium maintained at a temperature which is not more than a temperature of said molten metal; and 10  
 a driving mechanism for relatively moving said cooling member and said molten metal in order to agitate said molten metal by the aid of said cooling member. 15

21. The apparatus for producing said semisolidified metal according to claim 20, further comprising:

a first detecting means for detecting said temperature of said molten metal in said heat-insulating crucible; and  
 a second detecting means for detecting said temperature of said cooling medium. 20 25

22. The apparatus for producing said semisolidified metal according to claim 20, wherein said cooling mechanism includes:

a first supply means for supplying said cooling medium into said cooling member; and  
 a second supply means for supplying, into said cooling medium, a heating medium having a temperature higher than a liquefaction temperature of solidified matters, in order to remove said solidified matters adhered to a surface of said cooling member. 30 35

23. The apparatus for producing said semisolidified metal according to claim 22, further comprising a third detecting means for detecting a temperature of said heating medium. 40

24. The apparatus for producing said semisolidified metal according to claim 22, wherein said first supply means includes:

a first storage tank for storing said cooling medium; 45  
 a first heating section for keeping said temperature of said cooling medium in said first storage tank;  
 a heat exchanger for cooling said cooling medium by performing heat exchange with respect to said cooling medium; and 50  
 a first circulating passage for circulating said cooling medium to said first storage tank 55

through an interior of said cooling member.

25. The apparatus for producing said semisolidified metal according to claim 22, wherein said second supply means includes:

a second storage tank for storing said heating medium;  
 a second heating section for heating said heating medium in said second storage tank; and  
 a second circulating passage for circulating said heating medium to said second storage tank through an interior of said cooling member.

26. The apparatus for producing said semisolidified metal according to claim 22, wherein said cooling medium and said heating medium are melted metals.

27. An apparatus for producing semisolidified metal, comprising:

divided type heat-insulating crucibles for holding a predetermined amount of molten metal;  
 a cooling member for cooling said molten metal in said heat-insulating crucibles to a predetermined temperature;  
 a driving mechanism for driving said cooling member in said molten metal to agitate said molten metal; and  
 an opening/closing mechanism for driving said heat-insulating crucibles to open/close said heat-insulating crucibles so that said semisolidified metal is allowed to fall to be discharged after said molten metal is cooled and agitated in said heat-insulating crucibles to obtain said semisolidified metal.

28. The apparatus for producing said semisolidified metal according to claim 27, wherein said opening/closing mechanism includes:

a plurality of arm members for being detachably engaged with fastening means provided on side surfaces of said respective heat-insulating crucibles; and  
 a forward/backward moving means for moving said plurality of arm members back and forth in directions to make approach to one another and separation from each other.

29. The apparatus for producing said semisolidified metal according to claim 27, wherein said opening/closing mechanism includes:

a plurality of arm members for being detachably engaged with fastening means provided on



side surfaces of said respective heat-insulating crucibles; and

a swinging means for swinging said plurality of arm members in directions to make approach to one another and separation from each other. 5

30. The apparatus for producing said semisolidified metal according to claim 27, further comprising divided type crucible holders for accommodating said heat-insulating crucibles in a state of tight contact with each other, said crucible holder being provided with a heater for keeping an interior temperature of said heat-insulating crucibles. 10

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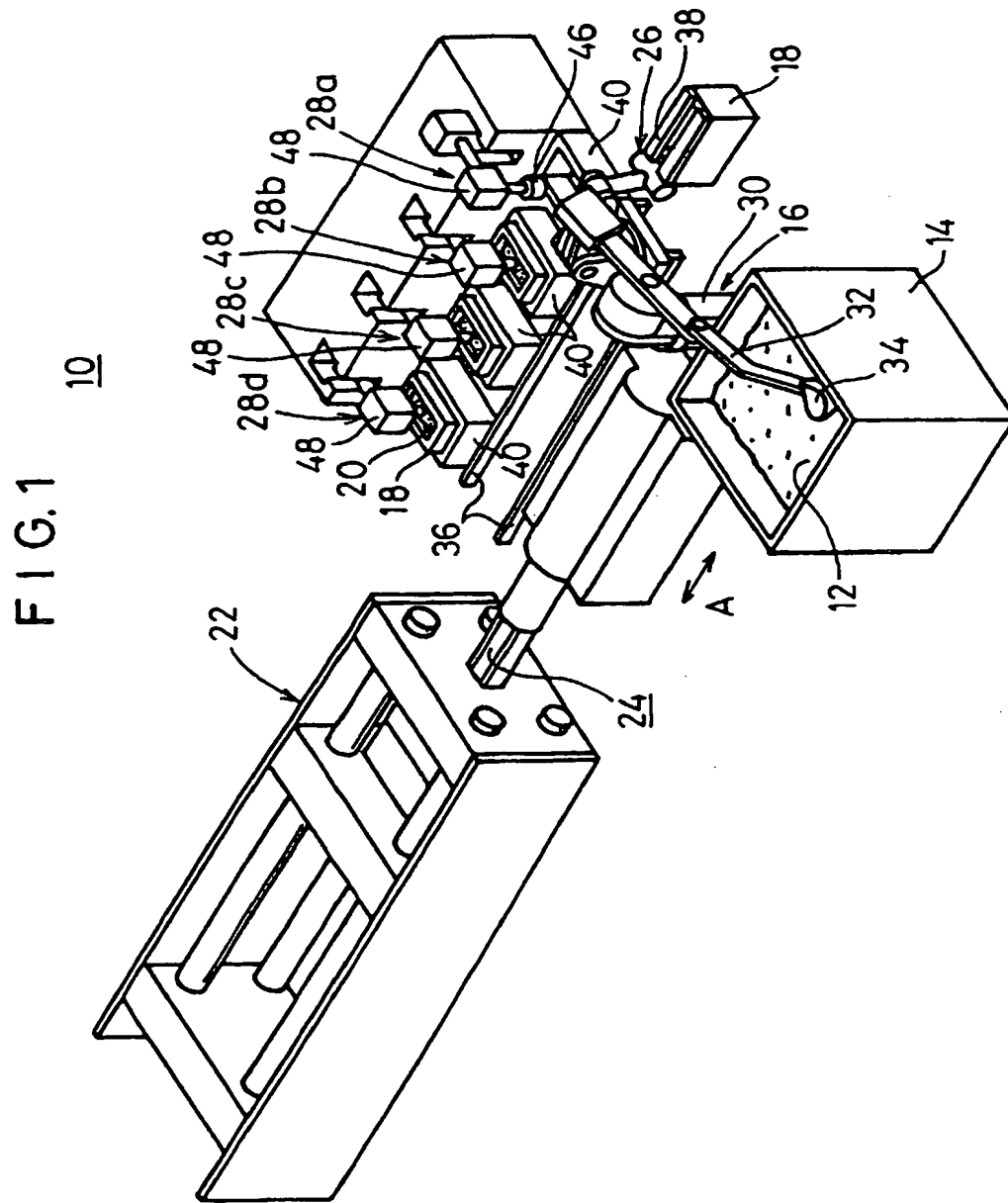




FIG. 3

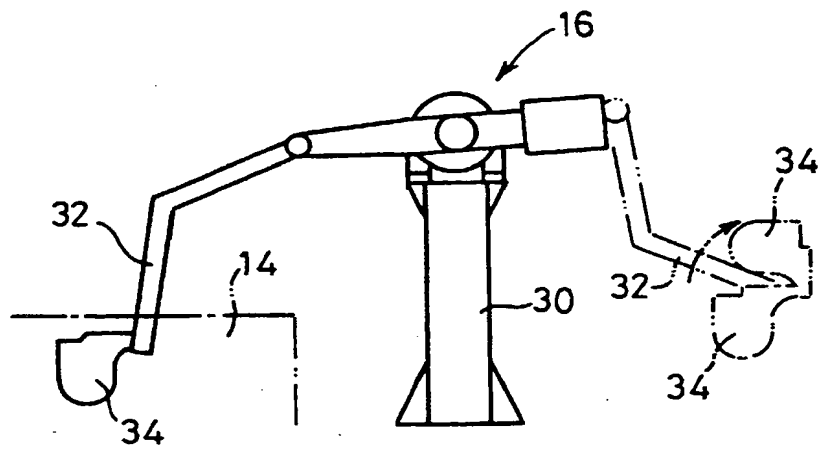
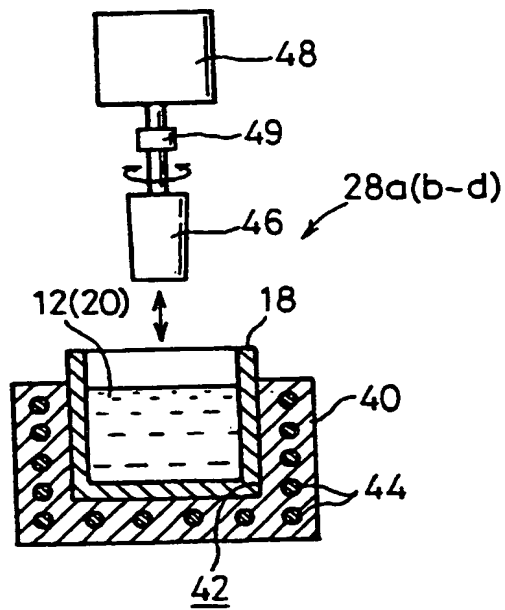


FIG. 4



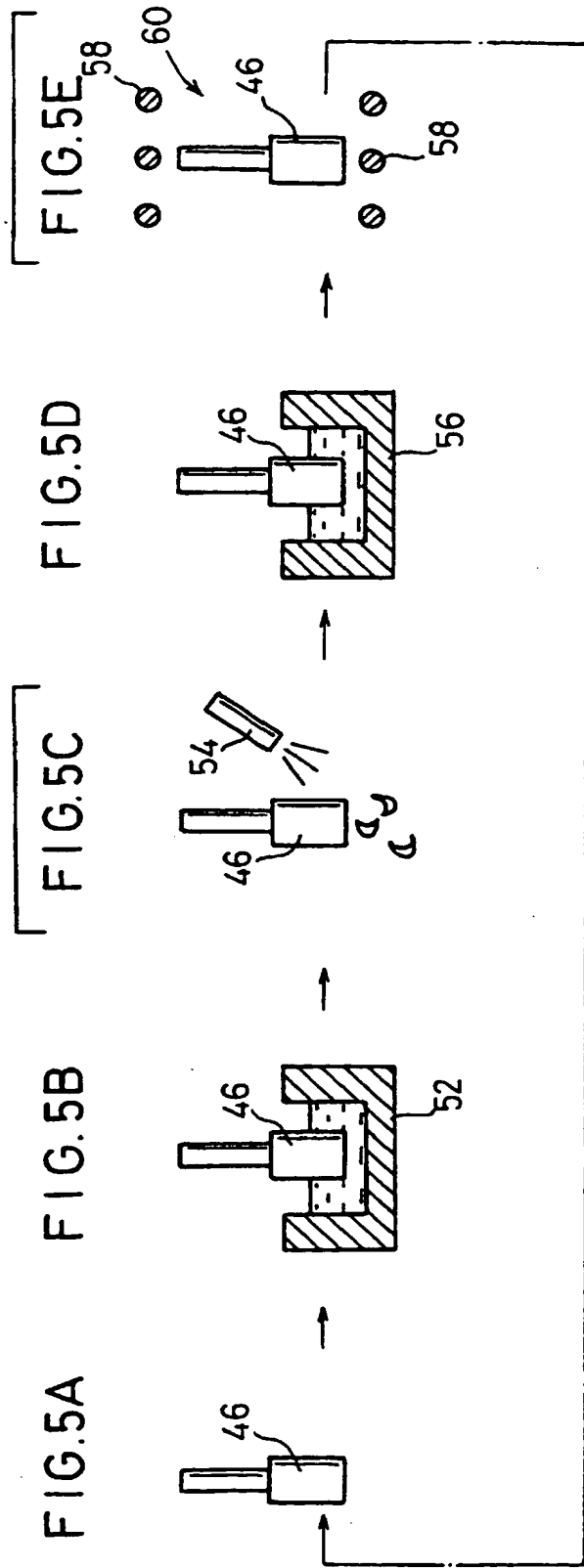


FIG. 6  
MASS PRODUCTION SYSTEM TIME TABLE

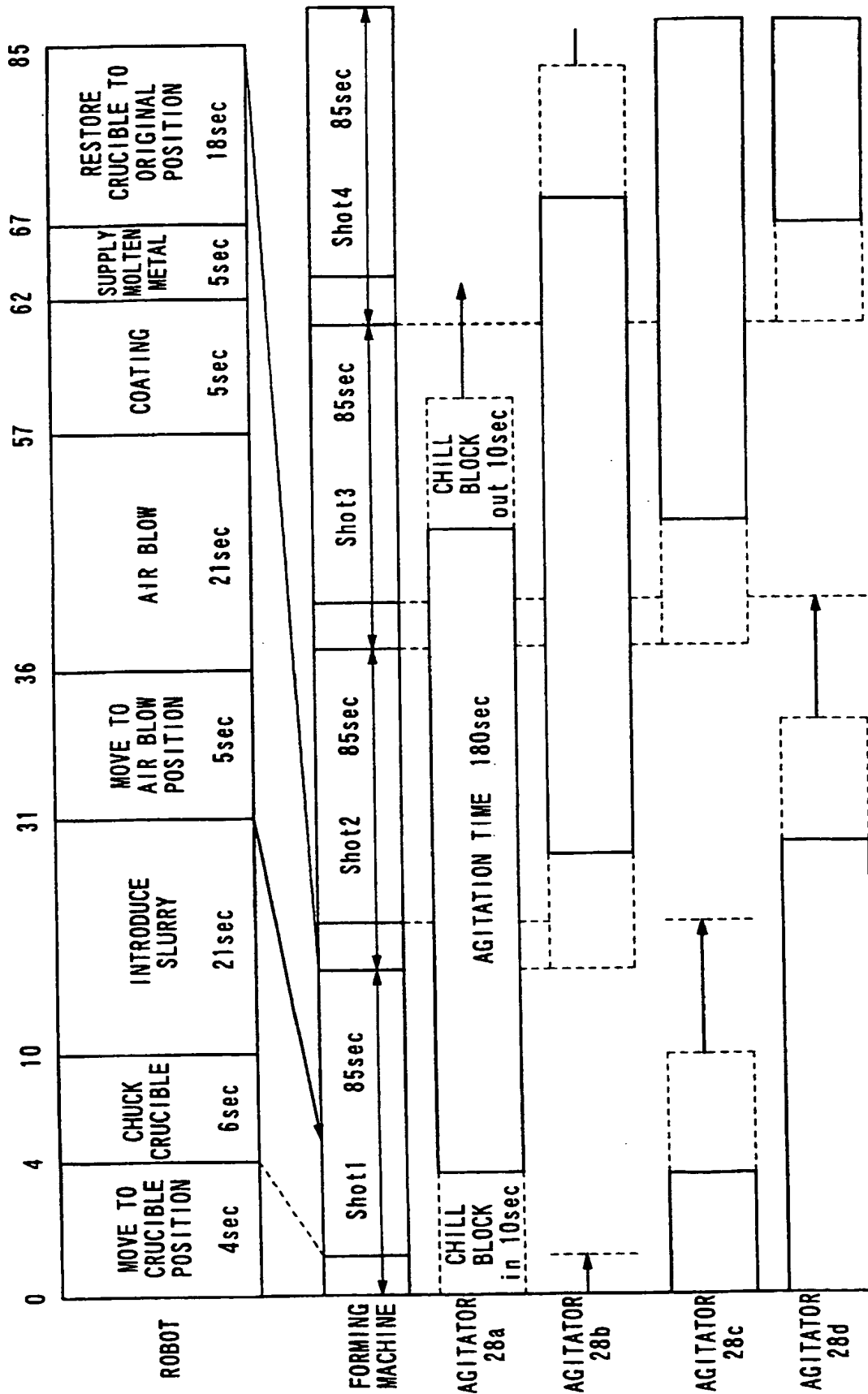


FIG. 7

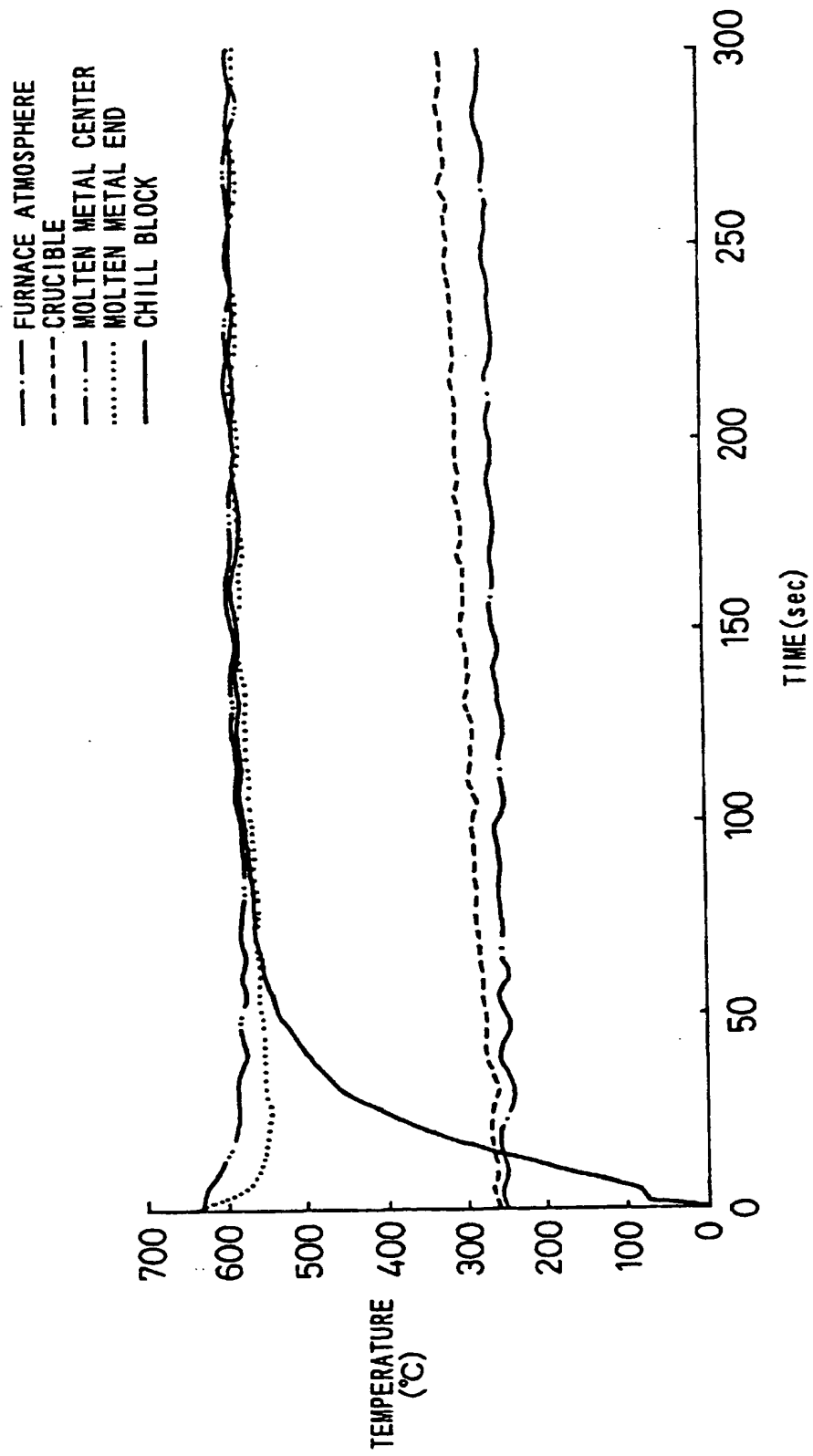




FIG. 8

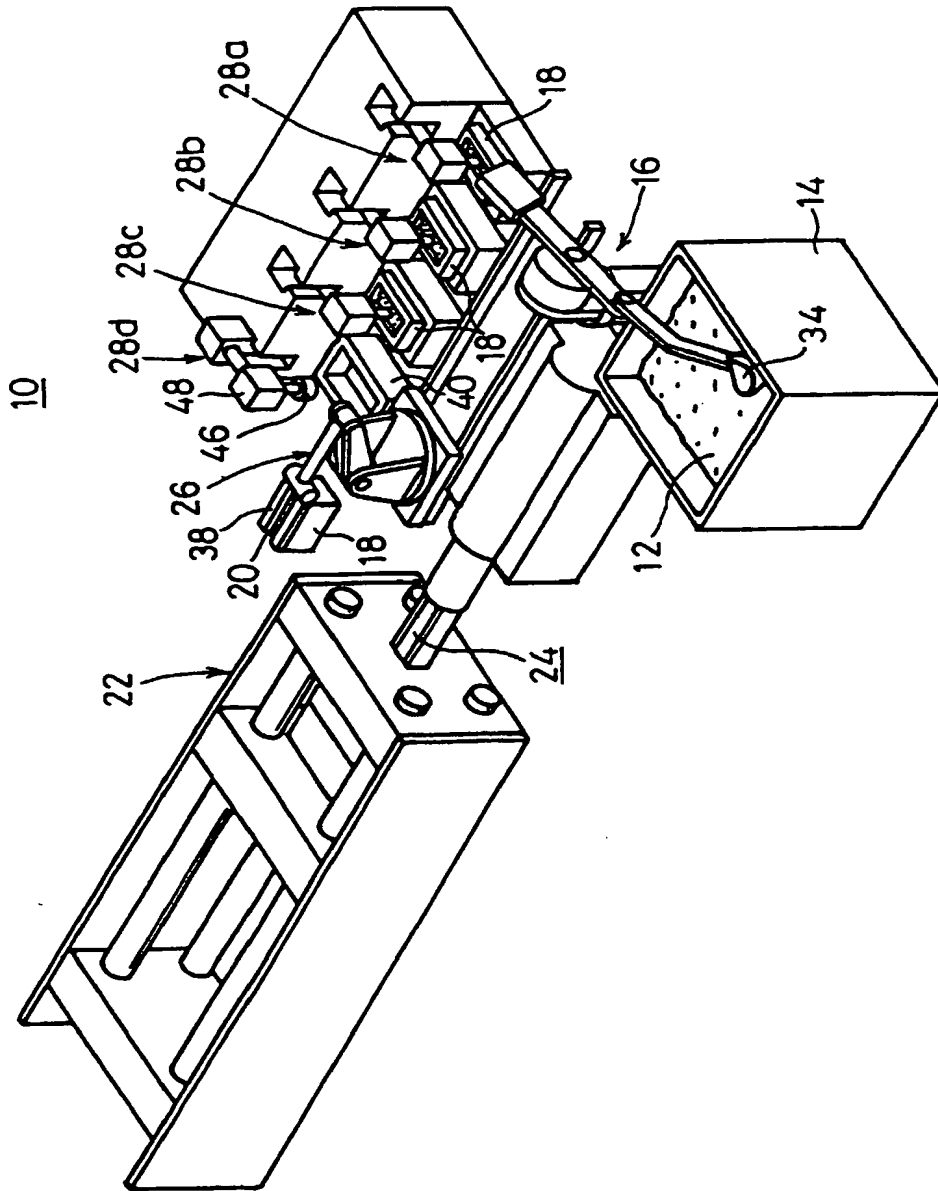


FIG. 9

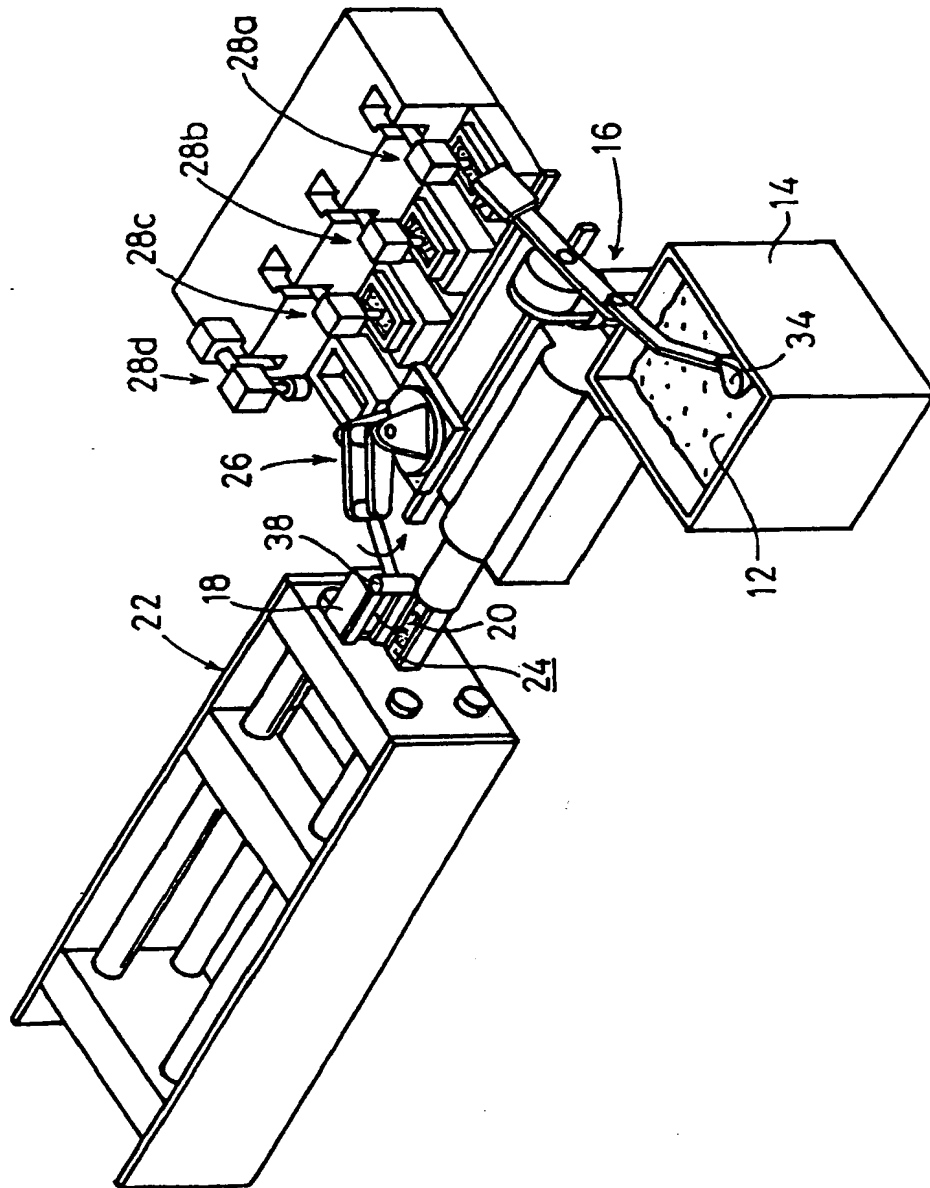
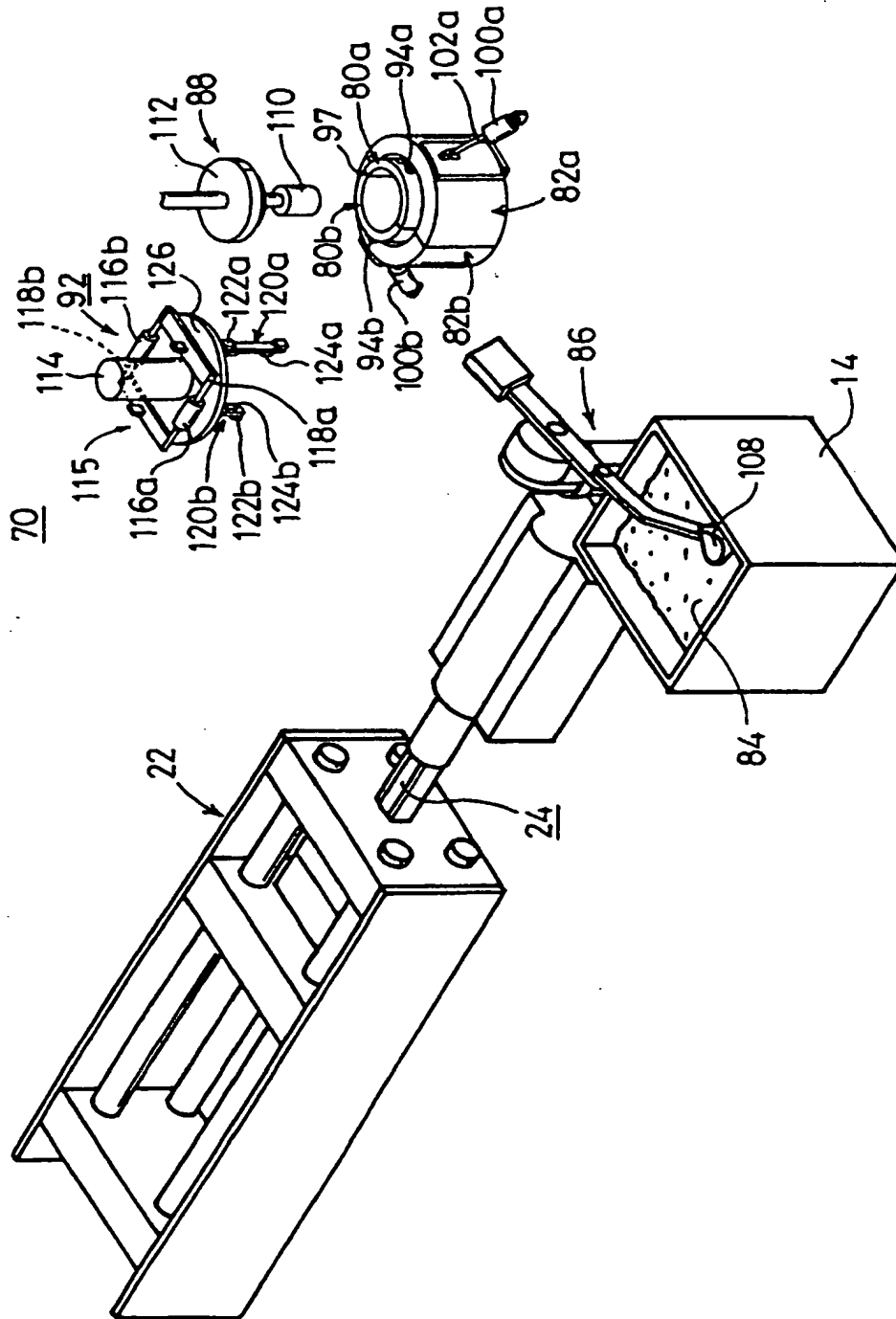


FIG.10



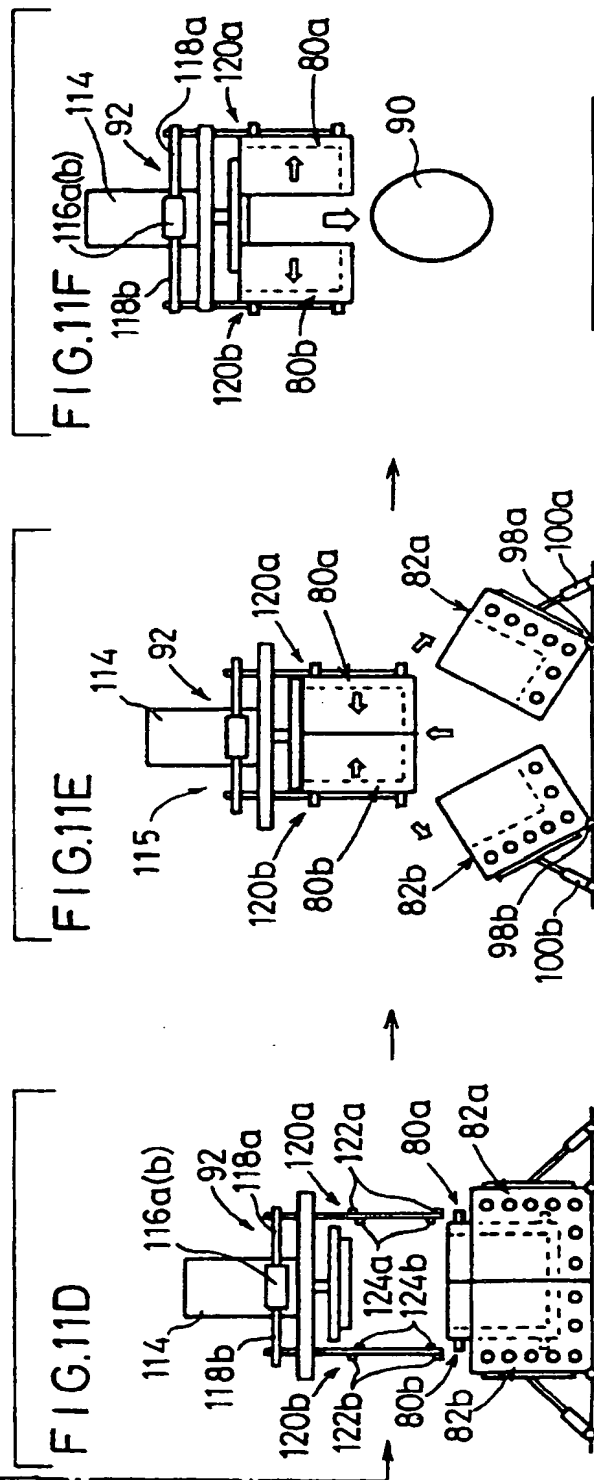
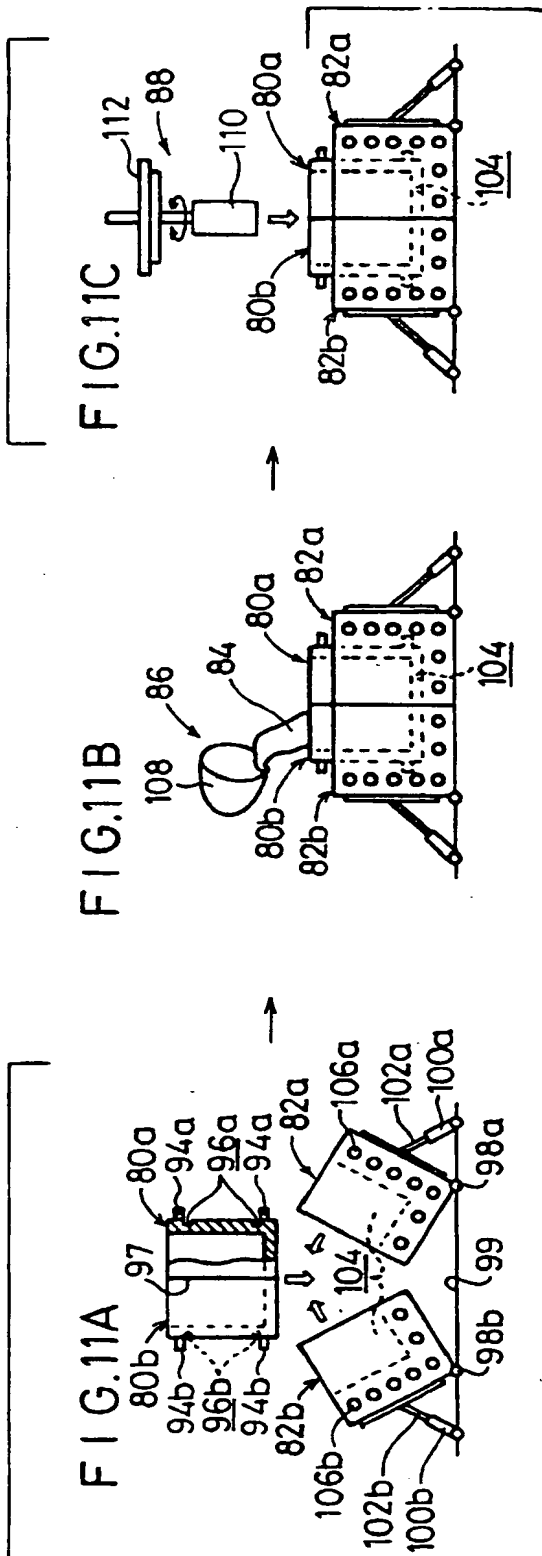
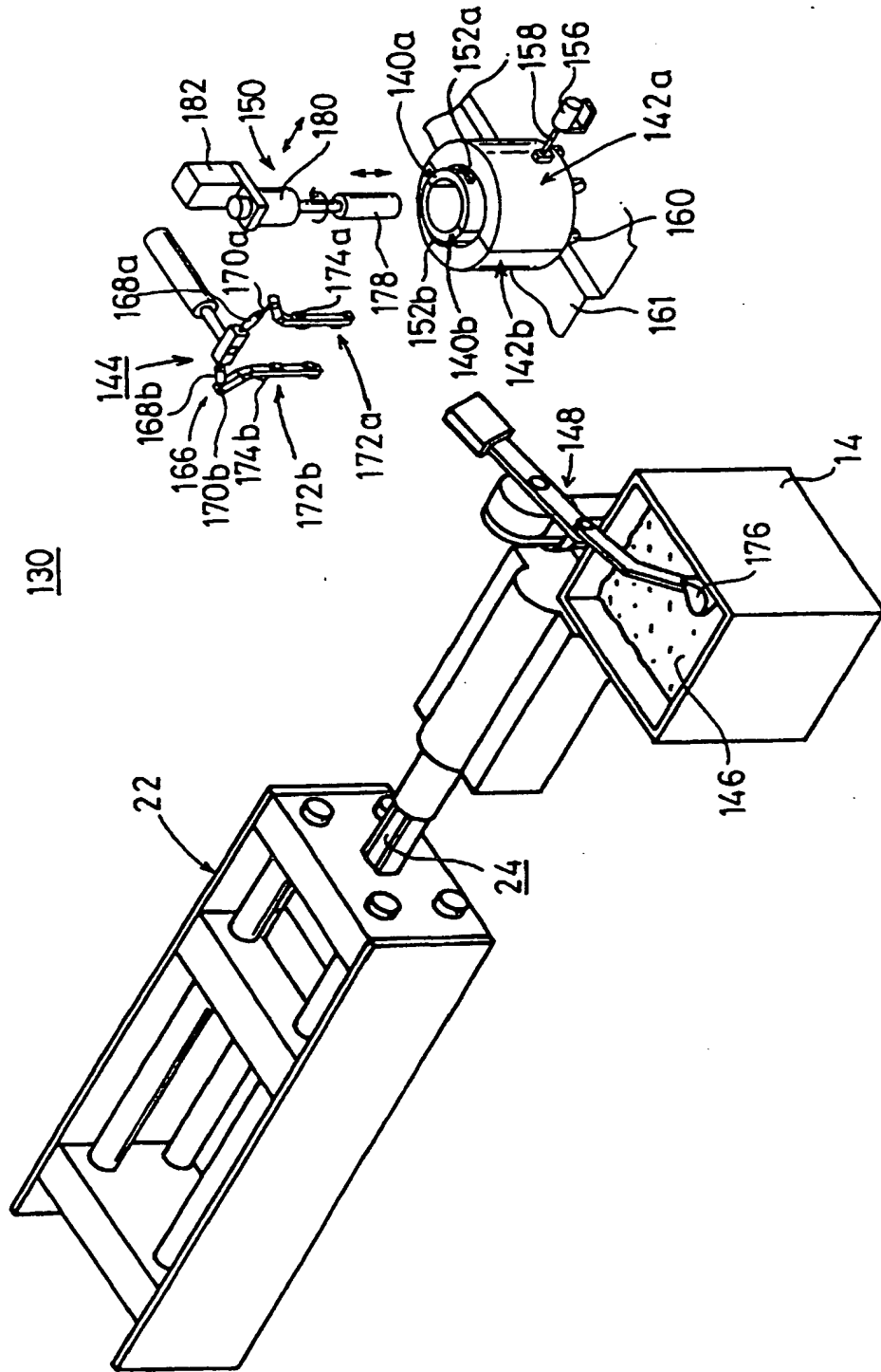


FIG.12



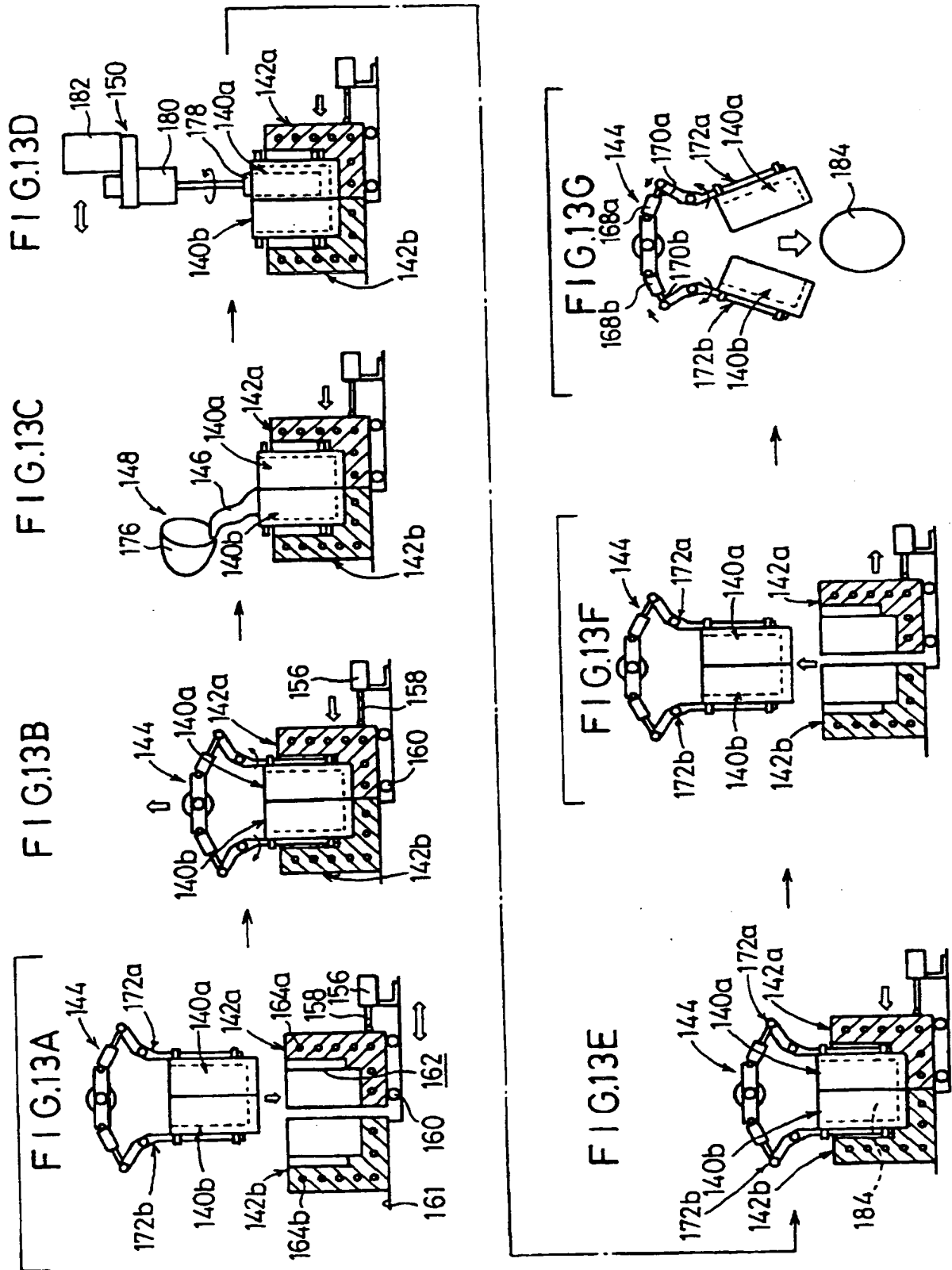


FIG.14

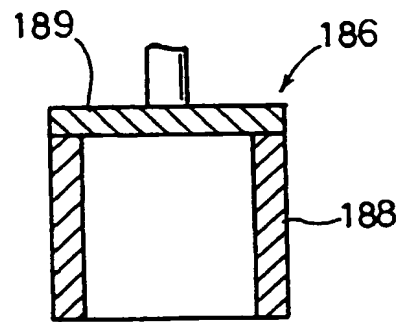
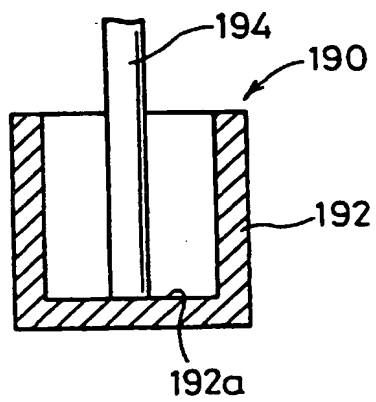


FIG.15



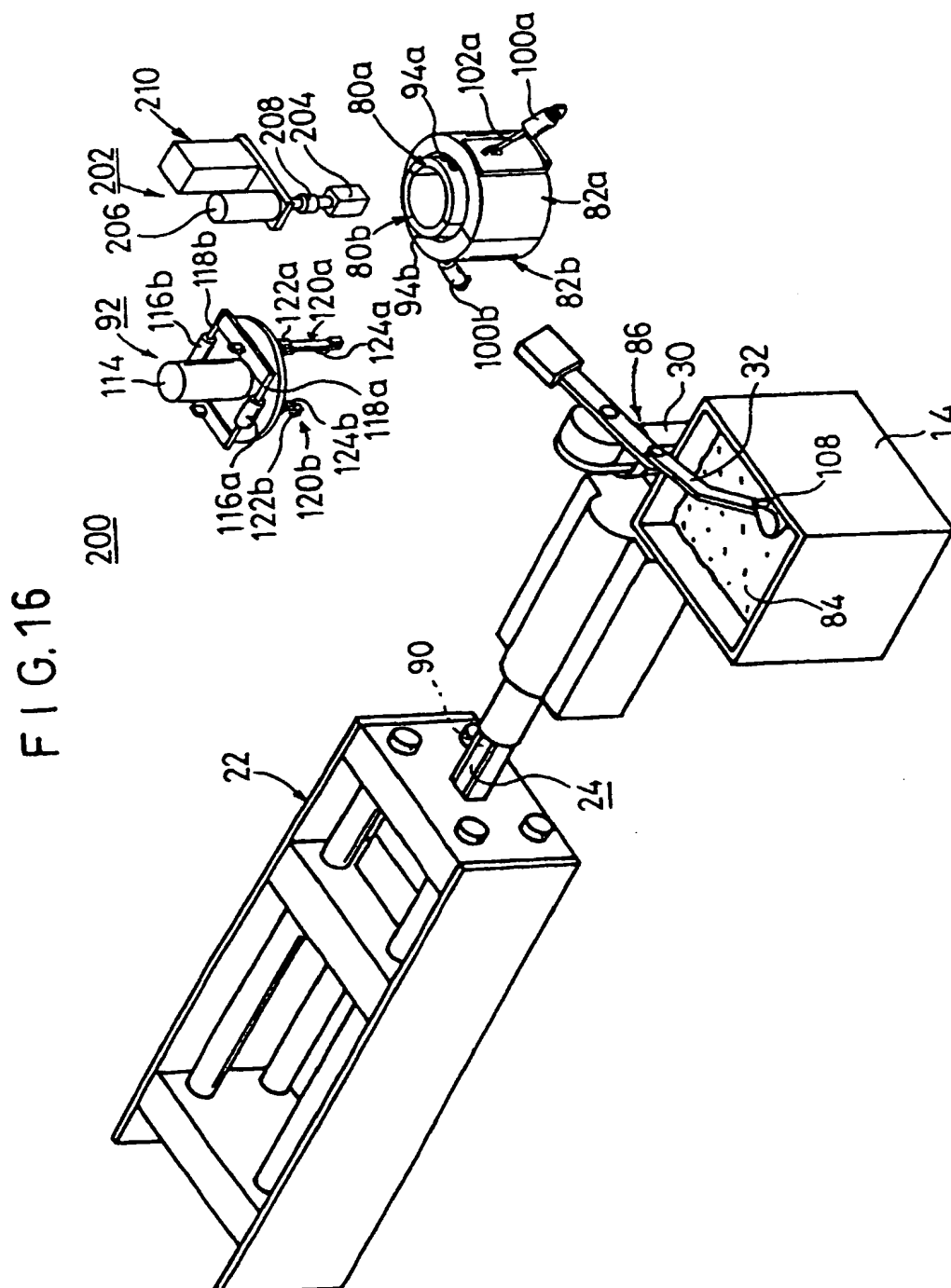




FIG. 17

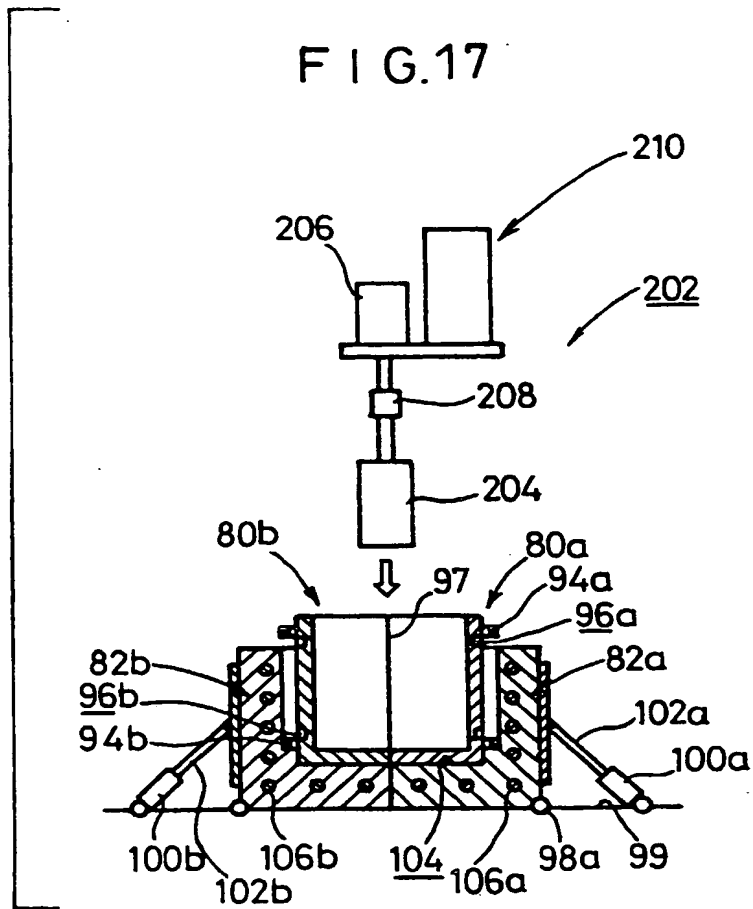
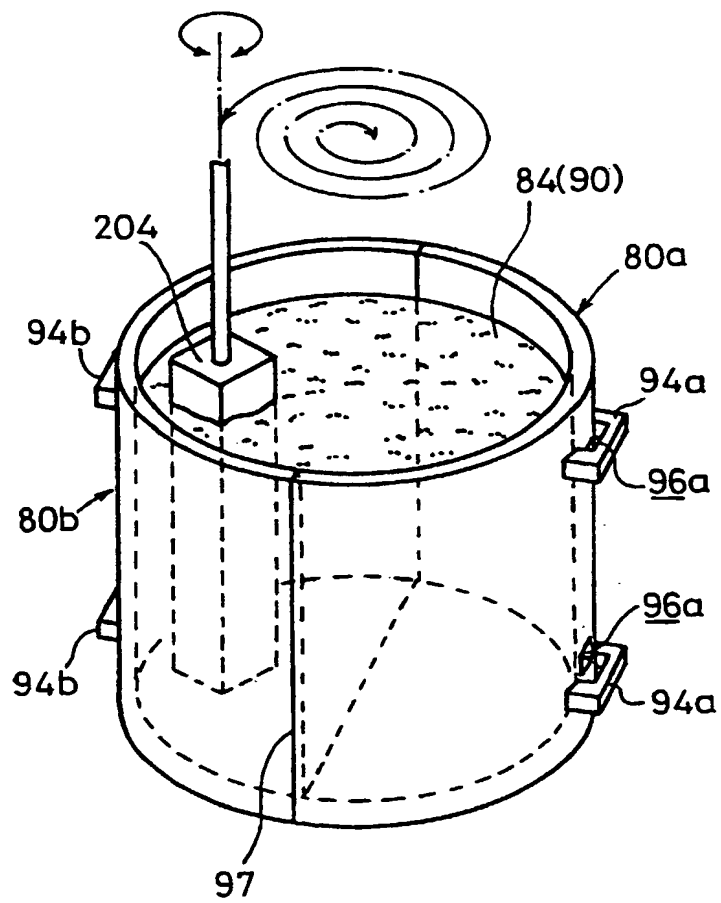


FIG.18



F I G.19

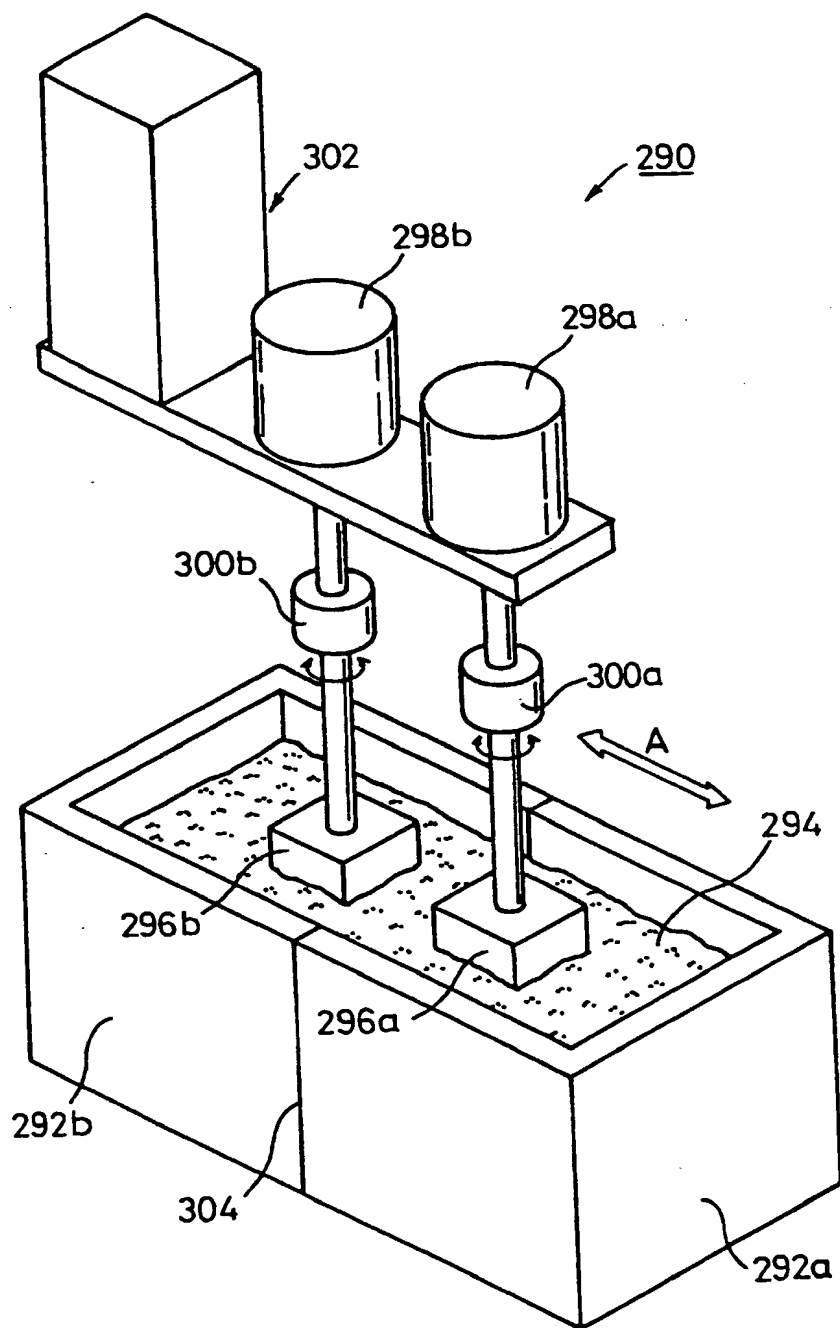


FIG. 20

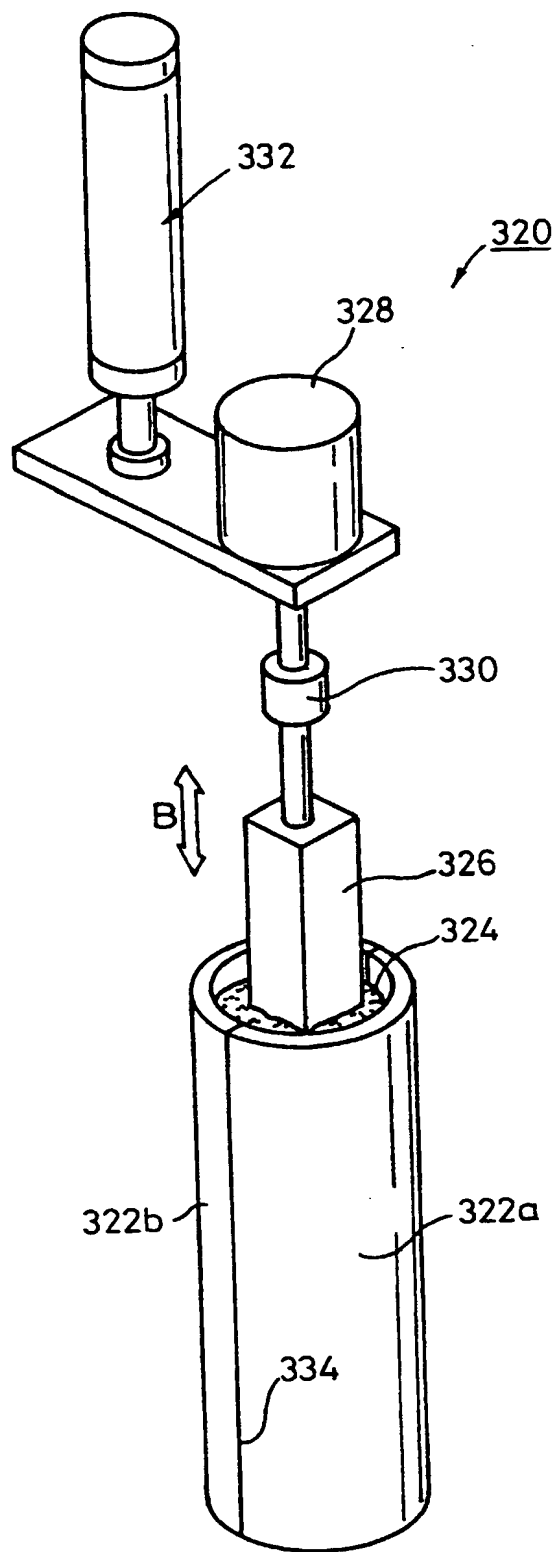


FIG. 21

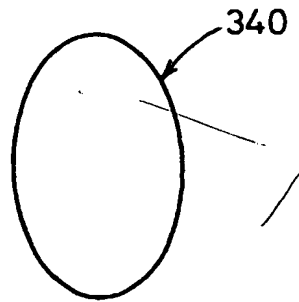


FIG. 22

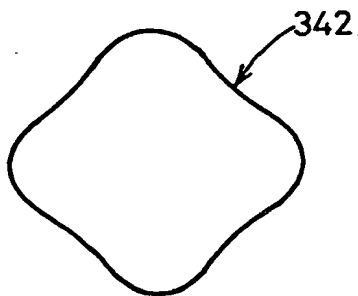


FIG. 23

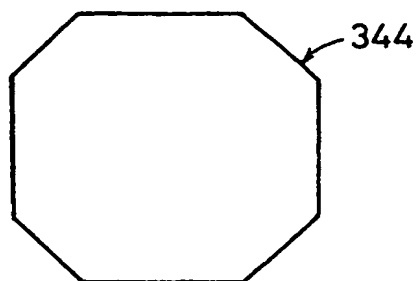


FIG. 24

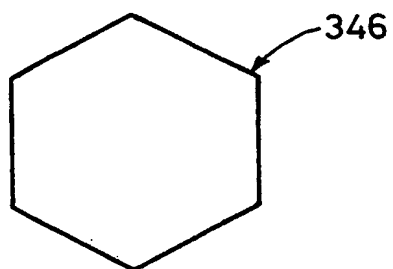


FIG. 25

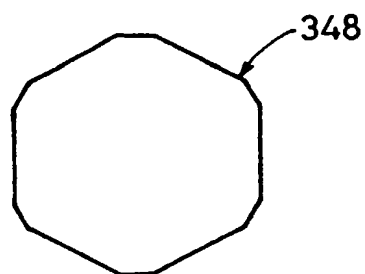


FIG. 26

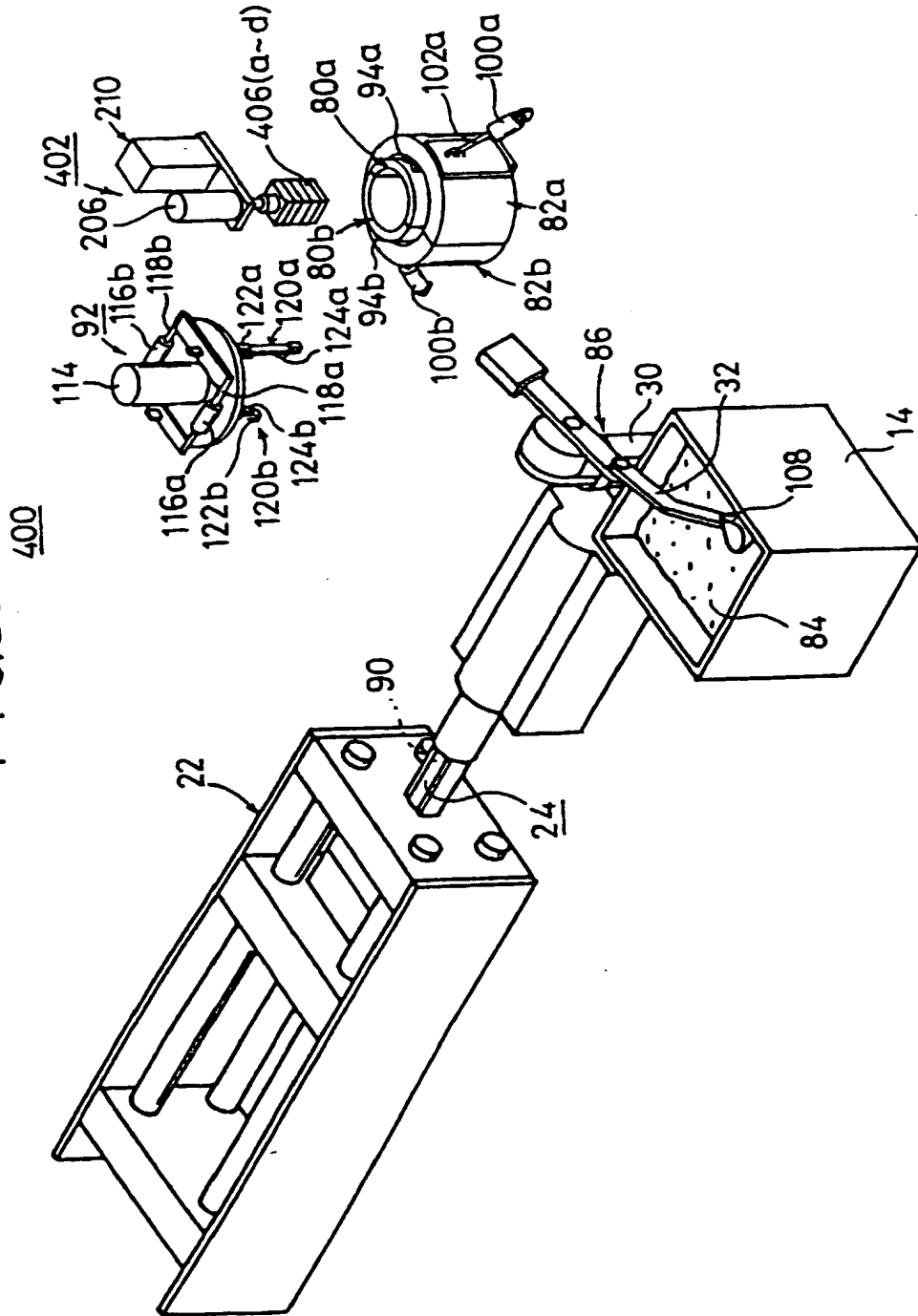


FIG.27

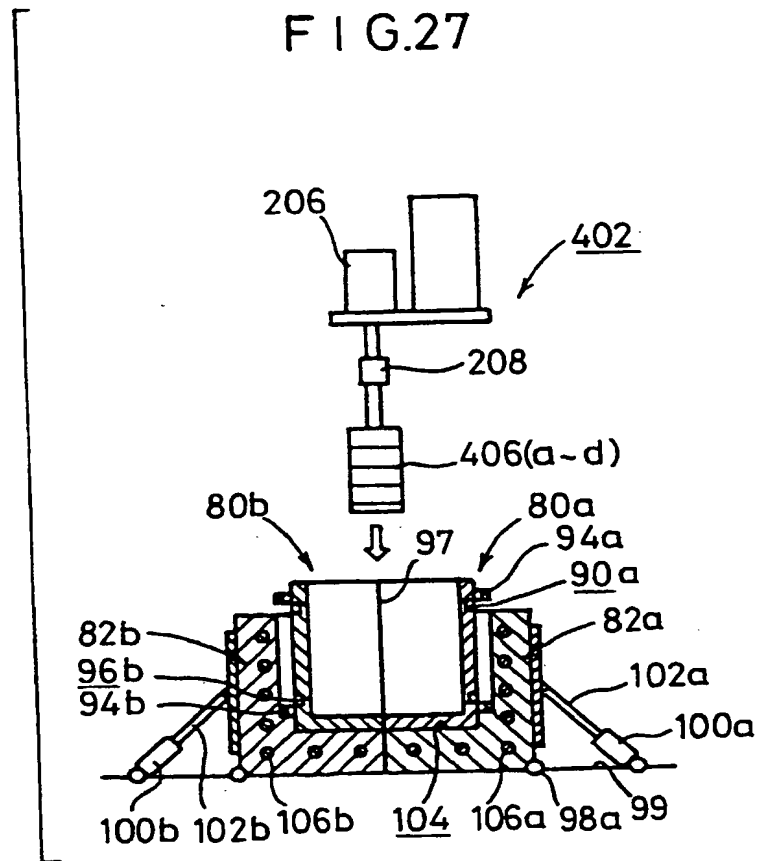




FIG. 28

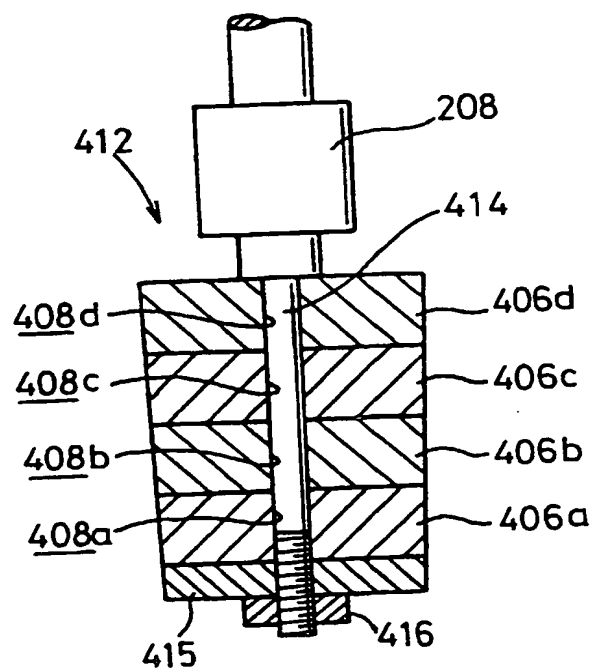


FIG. 29

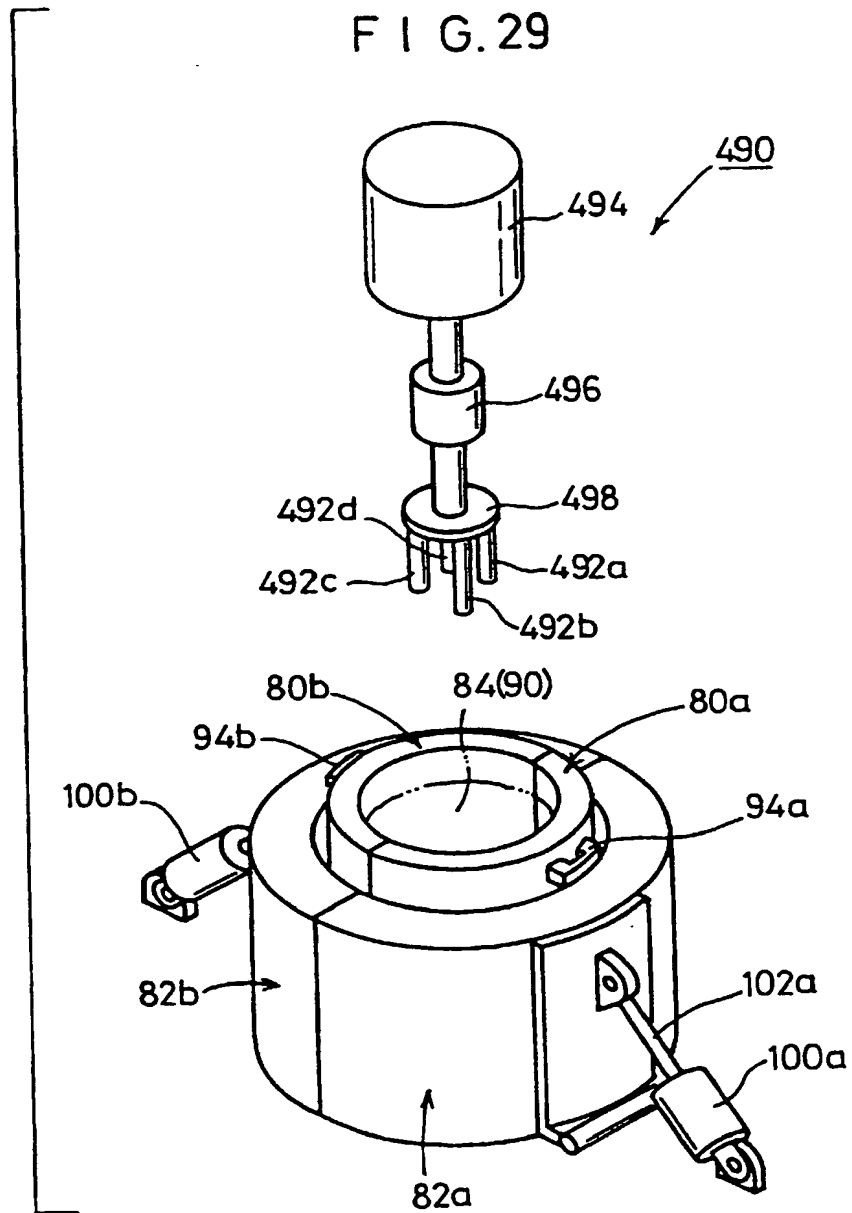


FIG. 30

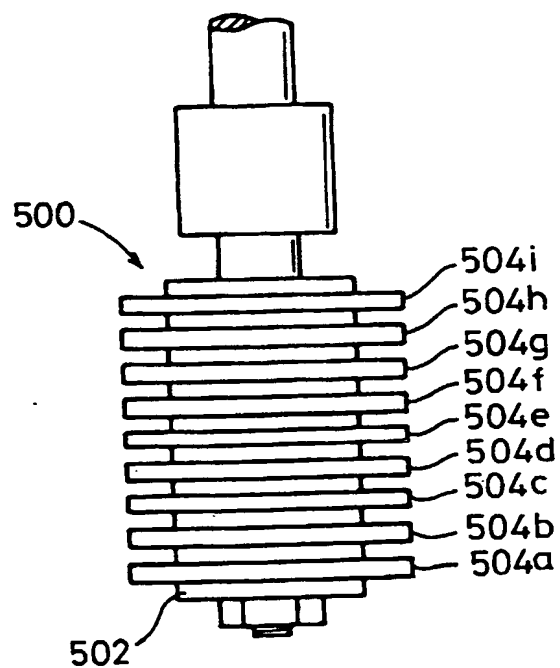


FIG. 31

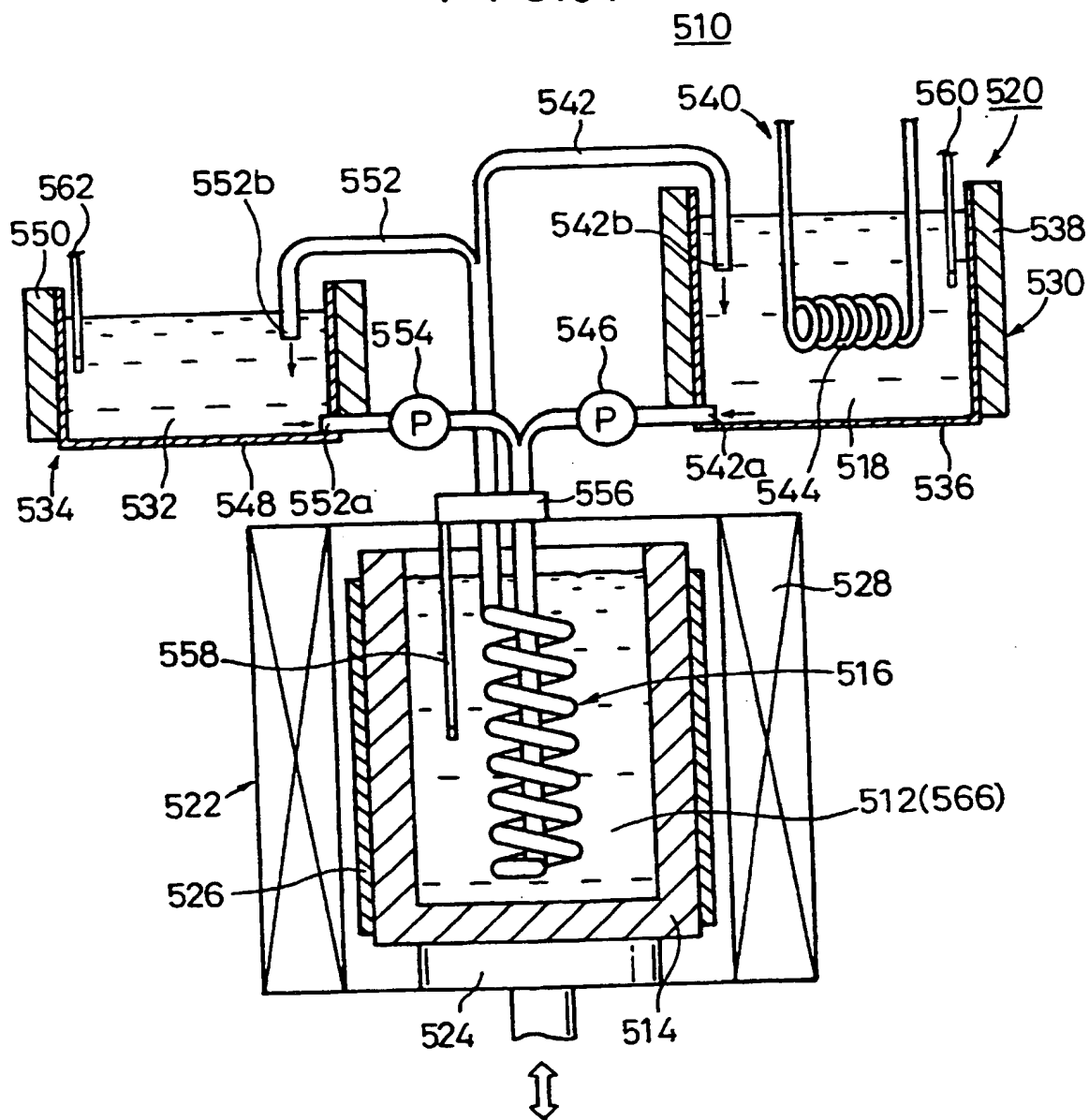


FIG. 32

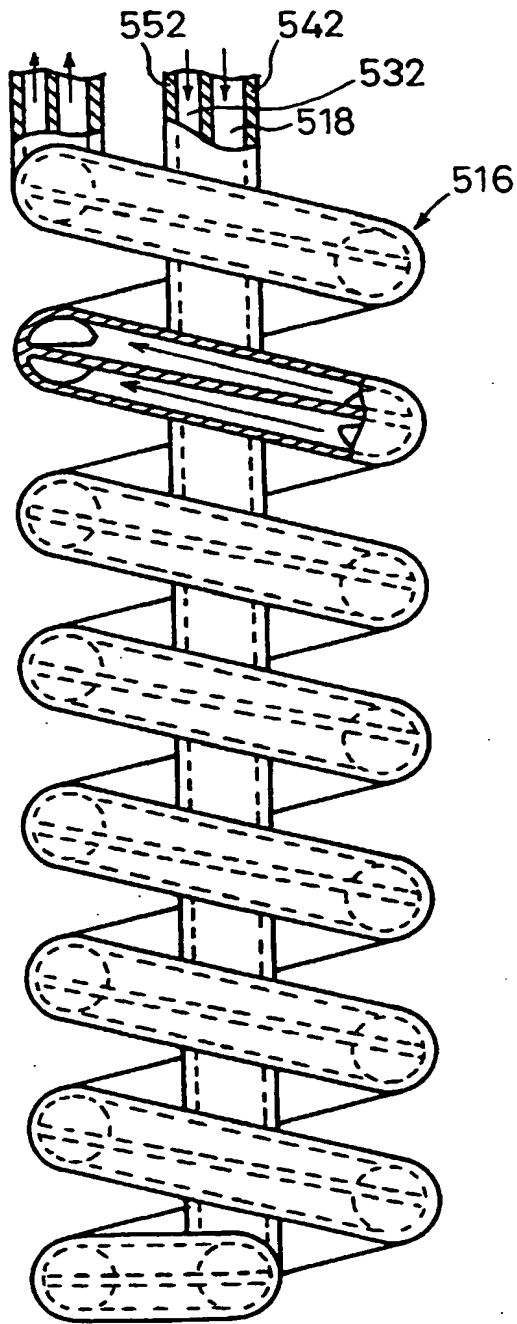


FIG.33A

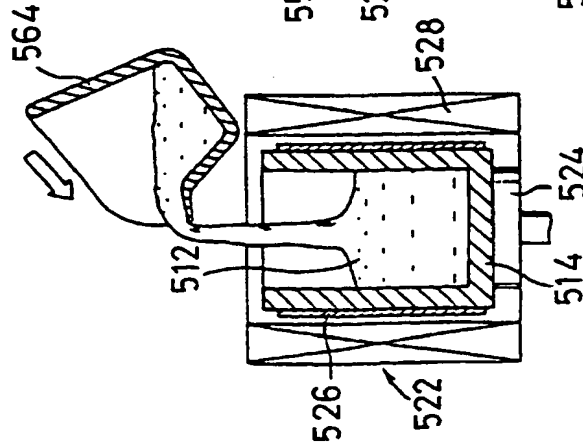


FIG.33B

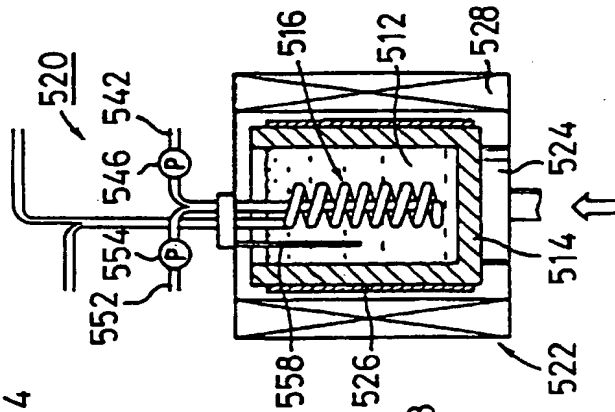


FIG.33C

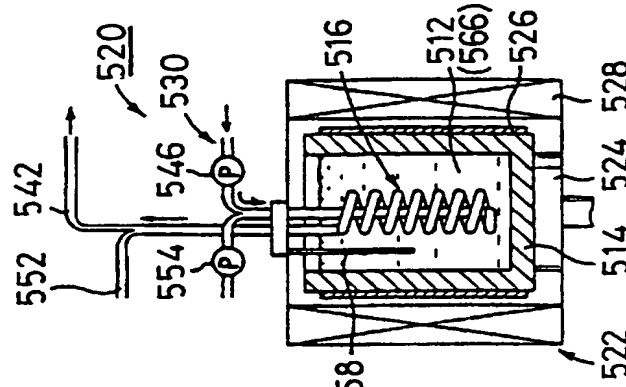
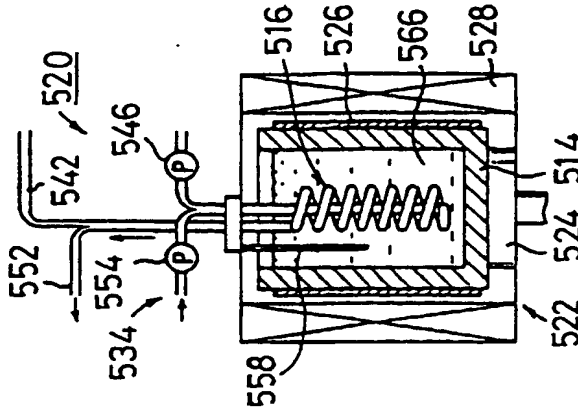


FIG.33D



## INTERNATIONAL SEARCH REPORT

International application No.

PCT/JP99/00163

<b>A. CLASSIFICATION OF SUBJECT MATTER</b> Int.Cl <sup>4</sup> B22D1/00, 17/30, C22C1/02		
According to International Patent Classification (IPC) or to both national classification and IPC		
<b>B. FIELDS SEARCHED</b>		
Minimum documentation searched (classification system followed by classification symbols) Int.Cl <sup>4</sup> B22D1/00, 17/30, C22C1/02, C22B9/02, F27B14/10		
Documentation searched other than minimum documentation to the extent that such documents are included in the fields searched Jitsuyo Shinan Koho 1926-1996 Toroku Jitsuyo Shinan Koho 1994-1999 Kokai Jitsuyo Shinan Koho 1971-1999 Jitsuyo Shinan Toroku Koho 1996-1999		
Electronic data base consulted during the international search (name of data base and, where practicable, search terms used)		
<b>C. DOCUMENTS CONSIDERED TO BE RELEVANT</b>		
Category*	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
Y A	JP, 3-162533, A (The Furukawa Electric Co., Ltd.), 12 July, 1991 (12. 07. 91), Page 1, left column, lines 5 to 14 ; page 2, lower left column, line 3 to lower right column, line 13 ; Fig. 1 (Family: none)	1, 2, 5-16, 19, 20, 27 3, 4, 17, 18, 21-26, 28-30
Y A	JP, 2-290931, A (Suzuki Motor Co., Ltd.), 30 November, 1990 (30. 11. 90), Page 2, upper right column, line 8 to lower right column, line 7 ; Fig. 2 (Family: none)	1, 2, 5-16, 19, 20, 27 3, 4, 17, 18, 21-26
Y	JP, 62-130234, A (Director General, Agency of Industrial Science and Technology), 12 June, 1987 (12. 06. 87), Page 3, upper left column, lines 6 to 12 ; Fig. 1 (Family: none)	5, 6 10, 15
Y	JP, 7-223047, A (Hitachi Cable, Ltd.), 22 August, 1995 (22. 08. 95), Column 1, lines 2 to 10 ; Fig. 1 (Family: none)	2, 11-14
<input checked="" type="checkbox"/> Further documents are listed in the continuation of Box C. <input type="checkbox"/> See patent family annex.		
* Special categories of cited documents: "A" document defining the general state of the art which is not considered to be of particular relevance "E" earlier document but published on or after the international filing date "L" document which may throw doubts on priority claim(s) or which is cited to establish the publication date of another citation or other special reason (as specified) "O" document referring to an oral disclosure, use, exhibition or other means "P" document published prior to the international filing date but later than the priority date claimed "T" later document published after the international filing date or priority date and not in conflict with the application but cited to understand the principle or theory underlying the invention "X" document of particular relevance: the claimed invention cannot be considered novel or cannot be considered to involve an inventive step when the document is taken alone "Y" document of particular relevance: the claimed invention cannot be considered to involve an inventive step when the document is combined with one or more other such documents, such combination being obvious to a person skilled in the art "<" document member of the same patent family		
Date of the actual completion of the international search 10 March, 1999 (10. 03. 99)		Date of mailing of the international search report 23 March, 1999 (23. 03. 99)
Name and mailing address of the ISA: Japanese Patent Office		Authorized officer
Facsimile No.		Telephone No.

Form PCT/ISA/210 (second sheet) (July 1992)

## INTERNATIONAL SEARCH REPORT

International application No.

PCT/JP99/00163

## C. (Continuation). DOCUMENTS CONSIDERED TO BE RELEVANT

Category*	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
Y	JP, 4-88135, A (Rheo-Technology Ltd.), 23 March, 1992 (23. 03. 92),	8, 16, 19
A	Page 2, lower left column, line 6 to lower right column, line 14 ; Figs. 1 to 3 (Family: none)	18
Y	JP, 7-185778, A (Sanja Denki Seisakusho K.K.), 25 July, 1995 (25. 07. 95),	27
A	Column 1, lines 2 to 9 ; Fig. 1 (Family: none)	28-30

Form PCT/ISA/210 (continuation of second sheet) (July 1992)



===== WPI =====

TI - Heating and transportation appts. for billet - where billet is received into bucket attached to revolving disc and billet is heated, removed from revolving disc and transferred to forming machine

AB - J08215819 In the heating and transporting appts. for a billet, a billet (W) is received into a bucket (5) removably attached to a revolving disc (2), and the billet (W) is heated at prescribed interval in the revolving locus of the bucket (5) by a heating device (3). The heated billet (W) in the bucket (5) is then removed from the revolving disc (2) and is transferred into a forming machine (1).

- ADVANTAGE - A billet is supplied into the forming machine in a heated state.

- (Dwg.1/5)

PN - JP8215819 A 19960827 DW199644 B22D17/00 005pp

PR - JP19950024992 19950214

PA - (HOND ) HONDA MOTOR CO LTD

MC - M22-G03D

DC - M22 P52 P53

IC - B21J1/06 ;B22D17/00 ;B22D17/30

AN - 1996-437786 [44]

===== PAJ =====

TI - DEVICE FOR HEATING AND CONVEYING BILLET

AB - PURPOSE: To secure the accuracy of relative position between a heating means and a billet and to heat the billet sufficiently by heating the billet under the condition of incorporating in a bucket and conveying the billet to a forming machine as this billet incorporates in the bucket.

- CONSTITUTION: In a heating and conveying device for billet W, plural buckets 5 incorporating the billet W are fitted in the constant pitch so as to be freely attachable/detachable to the front surface of a rotary plate 2 supported with a rotary shaft 22. The rotary plate 2 is intermittently rotated at the equal pitch as the arranged pitch of the bucket 5 with a driving means. The heating means 3 is adjacently arranged in the peripheral direction faced to a prescribed section of the revolutional locus of the buckets 5 to execute the continuous heating treatment of the billet W. When the bucket 5 shifts to the outlet side of the heating means 3, the bucket 5 is held up from a supporting member 24 by holding the handle part 5b of the bucket 5 with a holding tool 4a, and the billet W already heated is conveyed to the forming machine 1 together with the bucket 5 by the movement of a robot 4. The bucket 5 is overturned just above the hopper 12 and the billet W is charged into an injection sleeve 13.

PN - JP8215819 A 19960827

PD - 1996-08-27

ABD - 19961226

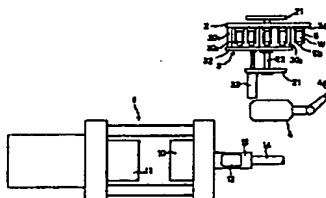
ABV - 199612

AP - JP19950024992 19950214

PA - HONDA MOTOR CO LTD

IN - ITO OSAMU;HIRONO HISAO;SUWA HIROYASU

I - B22D17/00 ;B21J1/06 ;B22D17/30



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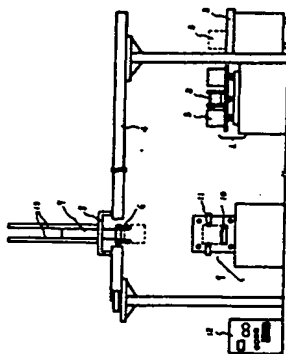
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===== WPI =====

- TI - Automatic mould exchange system for injection moulding - using appts. comprising supply of moulds, and guide rail and control unit for transfer of moulds to moulding machine
- AB - J56070925 The appts. has a mould stocker (1) for stocking moulds (3) for an injection moulding machine (9). A guide rail (4) is arranged between (1) and (9). A robot (5) is transferred along (4) with each (3). A control unit (12) controls (5). After (5) raises (3) from (1), they are moved to (9) via (4), then (3) is lowered onto (9) to exchange moulds.
- The moulds are automatically exchanged in several injection moulding machines.
- PN - JP56070925 A 19810613 DW198131 004pp
- JP58018899B B 19830415 DW198319 000pp
- PR - JP19790147051 19791115
- PA - (HITA ) HITACHI LTD
- MC - A09-D A11-B12C
- DC - A32 P53
- IC - B22D17/22 ;B29C1/16 ;B29F1/00
- AN - 1981-55903D [31]

===== PAJ =====

- TI - AUTOMATIC DIE EXCHANGE SYSTEM FOR INJECTION MOLDINGMACHINE
- AB - PURPOSE:To make die exchange unattended with ease and at a low cost by means of an overhead travelling die transporting robot adapted to automatically move in and out the die provided above a die stocker and an injection molding machine.
- CONSTITUTION:A robot mechanism 5 is travelled on a rial 4 and stopped above an injection molding machine. Then, with a chuck section 6 lowered, a die 3 is hoisted, carried onto a die stocker 1 and hung down to be taken into stock. Subsequently, the die 3 is hoisting carried onto the molding machine 9 and then, hung down to replace. The operation of the robots is automatically controlled with a control means 21. This requires no additional space for exchanging dies while facilitating frequent exchange of dies.
- PN - JP56070925 A 19810613
- PD - 1981-06-13
- ABD - 19810827
- ABV - 005135
- AP - JP19790147051 19791115
- GR - M085
- PA - HITACHI LTD
- IN - KATO HIROSHI; others: 01
- I - B29F1/00



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WPI

TI - Automatic pressure casting line for brake rings - includes twin furnaces and pneumatic lubricator capable of treating 150 rings simultaneously

AB - RU2009009 The automatic pressure casting line for brake rings has a caster (40 with a mould, a loader (1), a collector (10), and a rings heating furnace (2), a trimming press (6), a castings receiver (8), a distributor furnace, a melt dispenser, a mould lubricator (5), and a robotised conveyor (10). The manipulator double-acting clamps (17) and the five-section drum (10) have a guide and support platforms (not shown).

- USE - In systems with optimised lubricating oil temp.

- ADVANTAGE - Economy and ease of operation are increased.

- (Dwg.1/1)

PN - RU2009009 C1 19940315 DW199435 B22D17/00 005pp

PR - SU19904824321 19900508

PA - (AVTO-R) AVTOBAZ STOCK CO

- (VOLZ-R) VOLZHSK CAR WKS

IN - LUKIN V V; POLIENKO V P; ROMASH A N

MC - M22-G03D

DC - M22 P53

IC - B22D17/00

AN - 1994-284177 [35]

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